

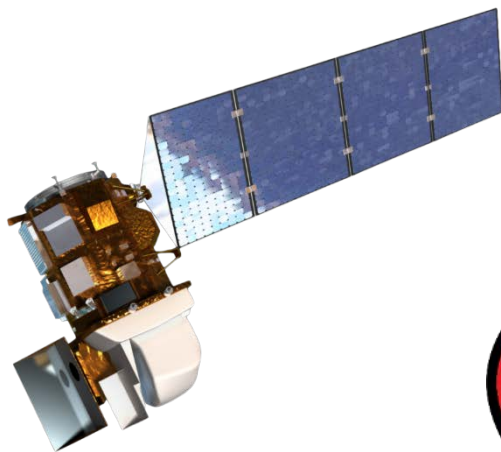


Initial Pre-Launch Imaging and Spectral Characterization of Landsat 9 Thermal Infrared Sensor-2

Aaron Pearlman¹, ²Joel McCorkel, Matthew Montanaro³, Boryana Efremova¹, Brian Wenny⁴, Allen Lunsford⁵, Amy Simon², Jason Hair², and Dennis Reuter²

¹GeoThinkTank LLC, ²NASA Goddard Space Flight Center, ³Rochester Institute of Technology, ⁴Science Systems and Applications, ⁵Catholic University of America

Calcon
Logan, Utah
June 18, 2018

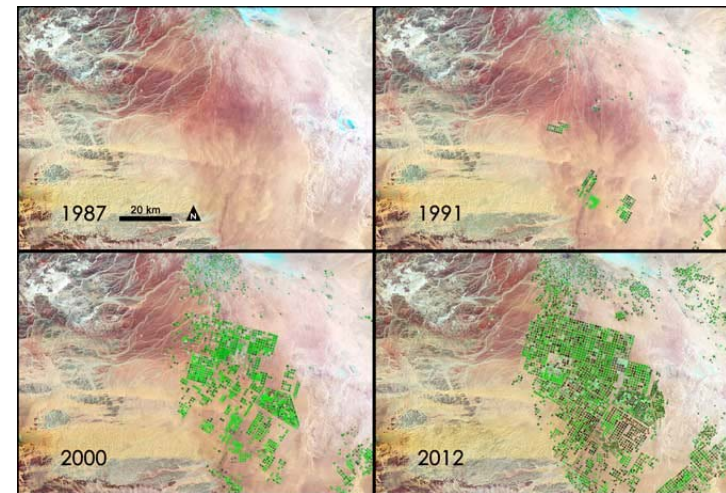
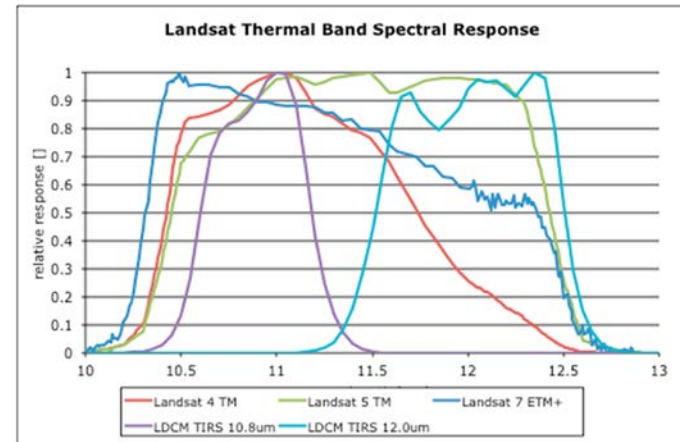




TIRS-2 Project Overview



- TIRS-2 will fly on the LandSat 9
 - 16 day re-visit cycle
 - 2 bands: 10.8 μm & 12 μm
- Like TIRS on Landsat 8, TIRS-2 will produce radiometrically calibrated, geo-located thermal image data
 - TIRS-2 operates in concert with, but independent of, the Operational Land Imager (OLI-2)
 - Final scene data generated as part of the Data Processing and Archive Segment at the United States Geological Survey/ Earth Resources Observation and Science (EROS) facility in Sioux Falls, South Dakota
- USGS responsible for operational code
 - TIRS-2 will deliver algorithms and parameters necessary to evaluate data and produce required outputs
 - No changes expected from process used for TIRS on Landsat 8
- TIRS-2 image data will have the same performance characteristics as that of TIRS on Landsat 8
 - Except better in some cases



– Increase in pivot irrigation in Saudi Arabia from 1987 to 2012 as recorded by Landsat. The increase in irrigated land correlates with declining groundwater levels measured from GRACE (courtesy M. Rodell, GSFC)

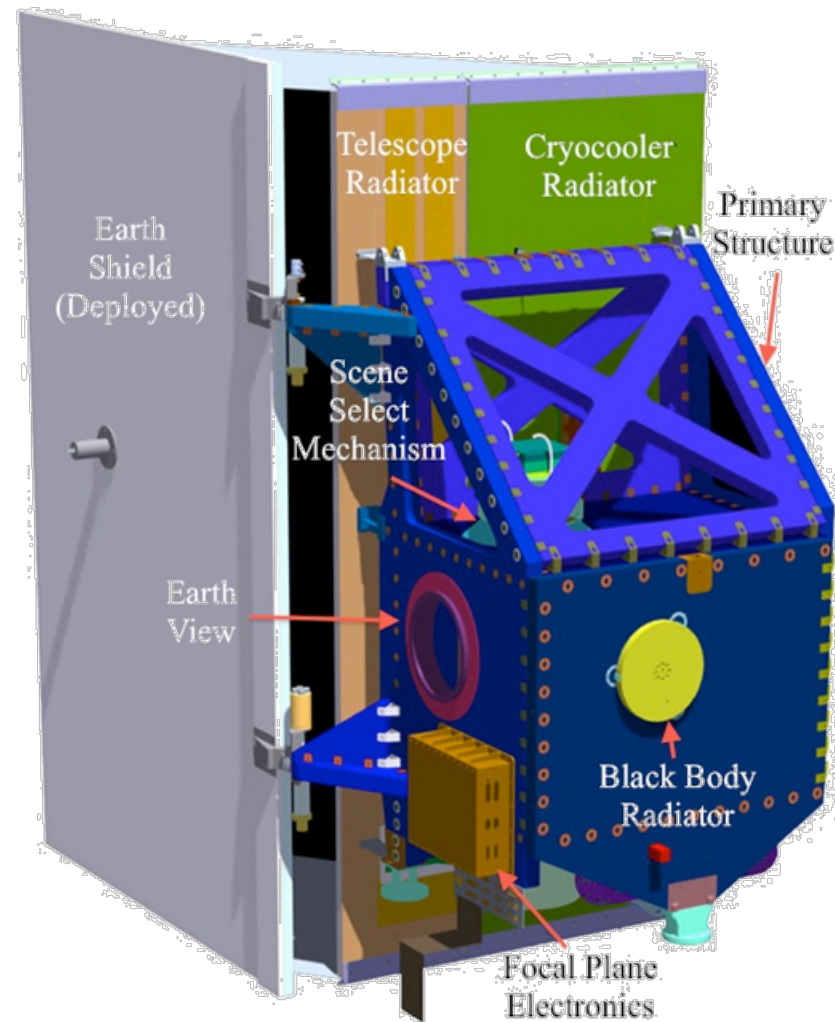
TIRS-2 will be a rebuild of Landsat 8 TIRS except TIRS-2 will be upgraded from Risk Class C to Class B for Landsat 9

TIRS-2 Improvements

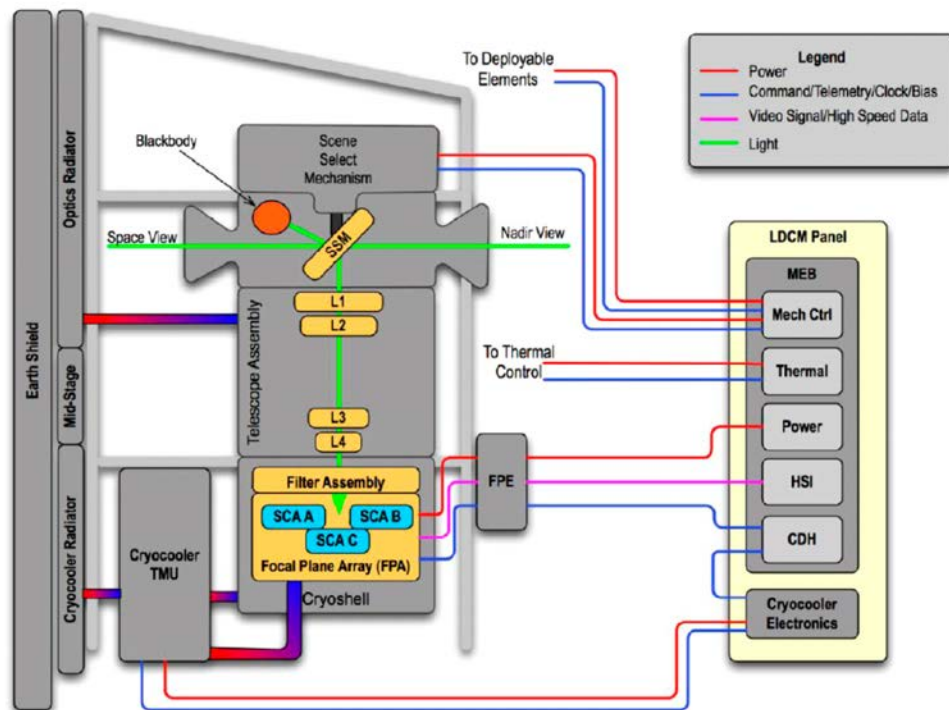
- Increased redundancy to satisfy Class B reliability standards
- Improved stray light performance through improved telescope baffling
- Improved position encoder for scene select mirror to address problematic encoder on Landsat 8 TIRS

TIRS-2 Status

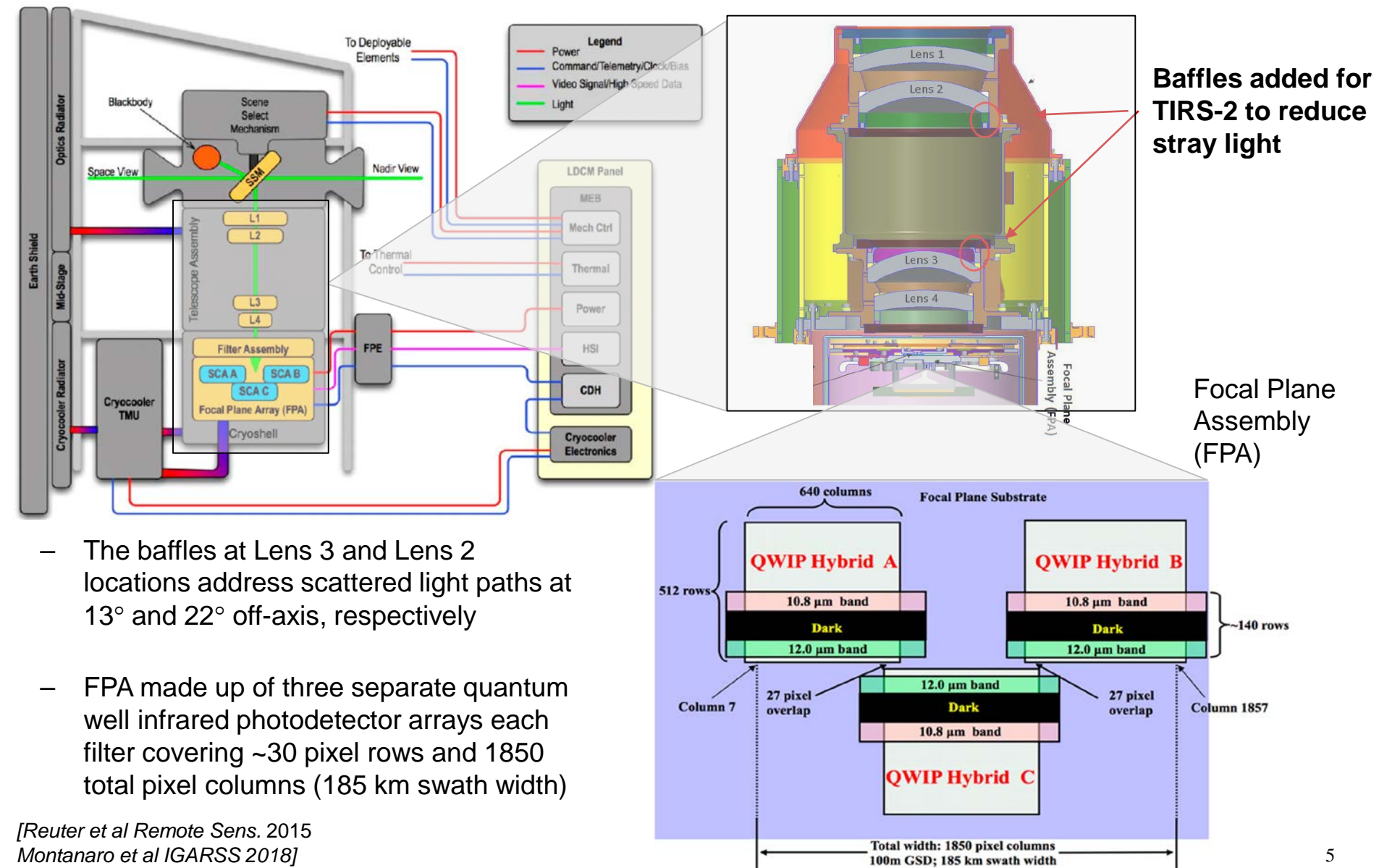
- NASA GSFC TIRS-2 team formed in 2015
- TIRS-2 successfully completed Critical Design Review in February 2017
- Instrument in fabrication at NASA GSFC
- **Initial pre-launch imaging and spectral characterization Nov. 2017 – March 2018**
- On target for August-2019 delivery to spacecraft



TIRS-2 Architecture



TIRS-2 Architecture



- The baffles at Lens 3 and Lens 2 locations address scattered light paths at 13° and 22° off-axis, respectively
- FPA made up of three separate quantum well infrared photodetector arrays each filter covering ~30 pixel rows and 1850 total pixel columns (185 km swath width)



Initial Pre-Launch Imaging and Spectral Characterization: aka TIRS-2 Imaging Performance & Cryoshell Evaluation (TIPCE)

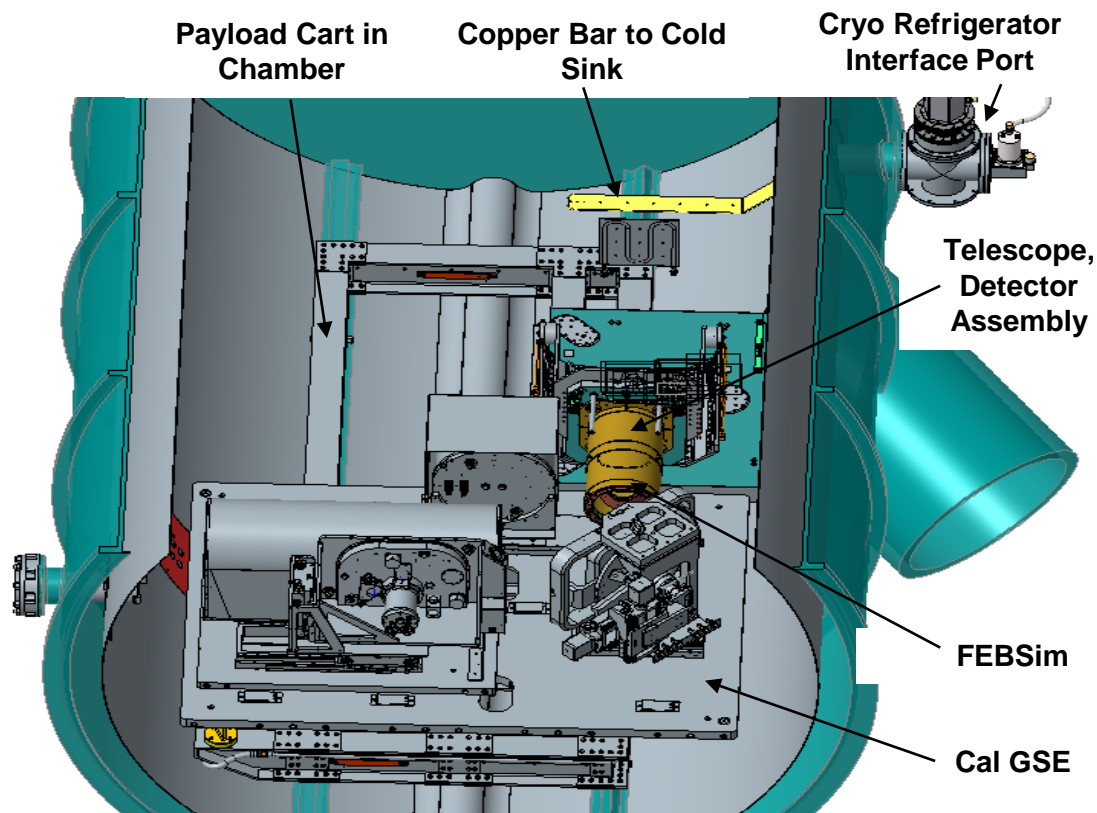


**Initial performance tests at “almost” instrument-level
(Telescope/focal plane arrays/focal plane electronics, no scene
select mirror)**

- Focus test
 - Determine focus position of FPA/telescope, determine proper shims, & verify
- Spatial response test - Initial characterization
- Far-field scatter test
 - Only opportunity to measure far-field scattering (due to config of test article and CGSE in the chamber)
- Spectral response test - Initial characterization
- Characterize cryoshell performance

TIPCE Chamber Configuration

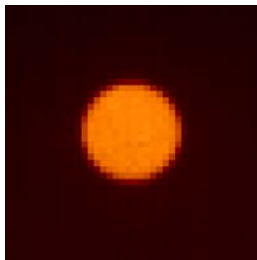
- Test article consists of major TIRS-2 components (except scene select mirror)
- Front end baffle simulator (FEBSim) forward of telescope to simulate entrance apertures of the optical system
- Test article positioned close to the calibration ground support equipment (Cal GSE) to allow for angular range needed for scatter survey.



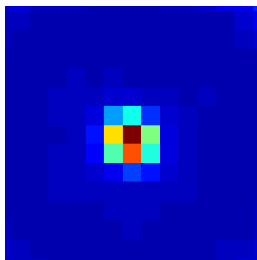
Top Down, Cutaway View of
Thermal Chamber

TIPCE Configuration

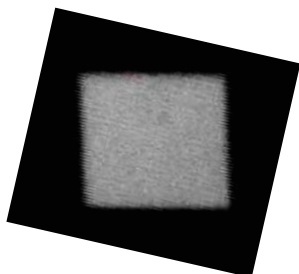
Focus, Scatter, & Spatial



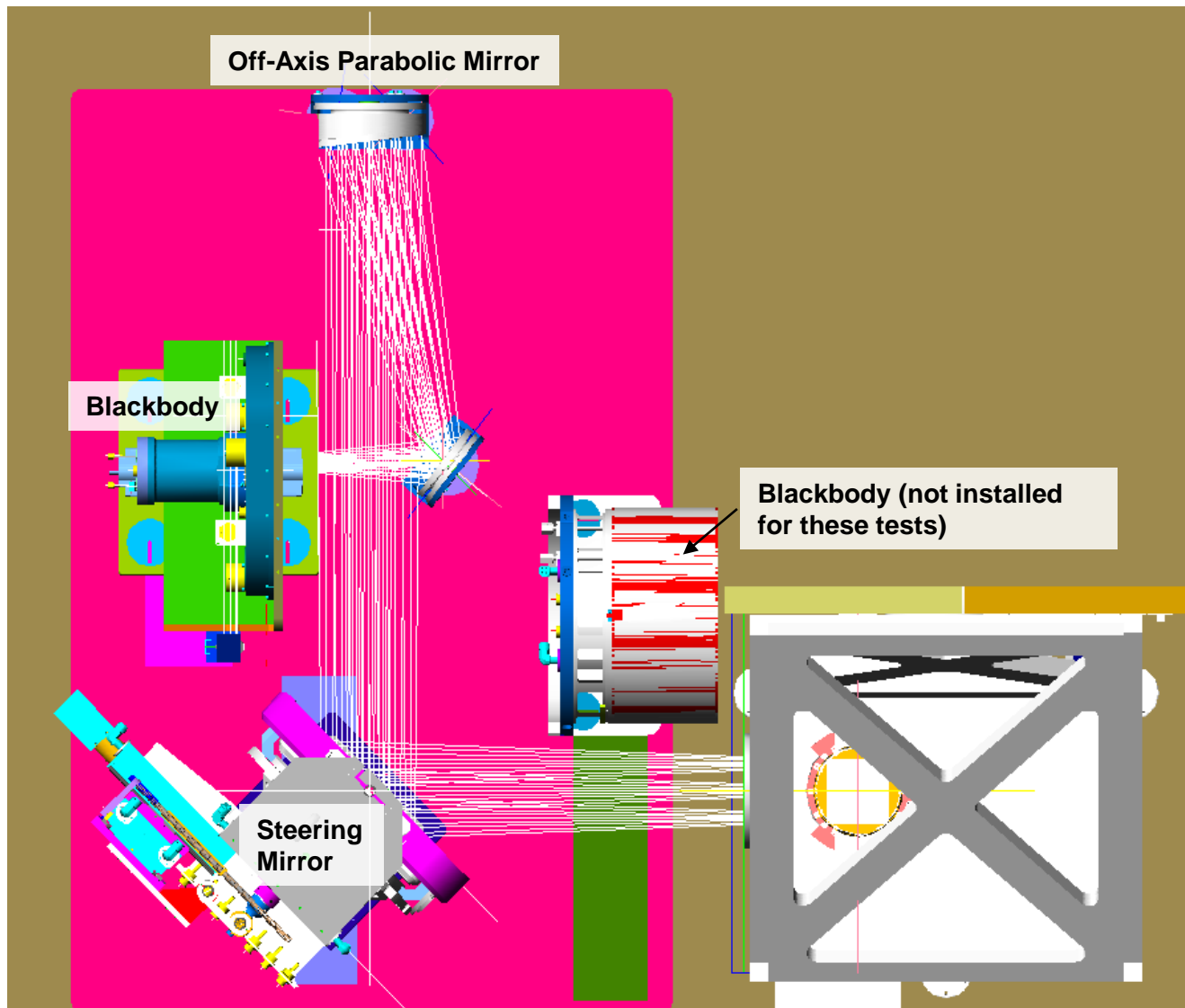
16-pixel circular target



1- and 2-pixel
circular targets



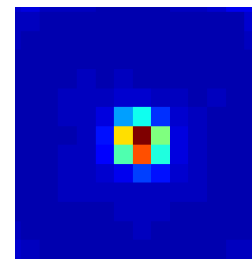
1-degree target



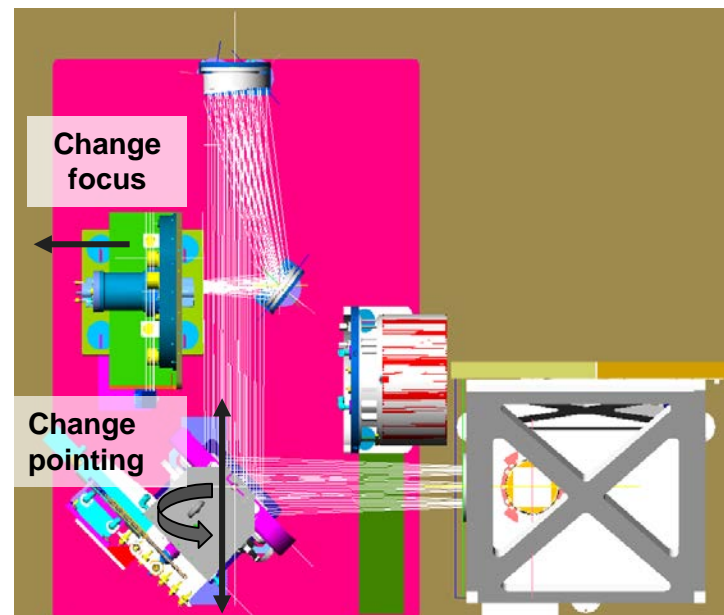
Focus Test Methodology

- The Focus Test is used to determine the optimal focus position of the TIRS-2 focal plane assembly (FPA) relative to the optical telescope.
- Optimal focus is determined by minimizing the full-width, half-maximum (FWHM) of a Gaussian-based model fit to the image created by an input two-pixel source.
- ***This focus map is then reported to the instrument team so that proper shims can be fabricated and installed.***
- These measurements are first performed at the telescope-FPA assembly (TIPCE level) to find best focus, then repeated at the full instrument level to validate consistency and characterize focus as function of telescope temperature.

Two-Pixel Source

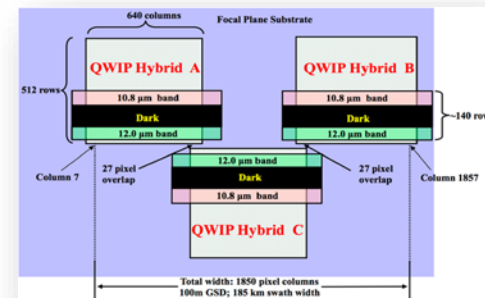
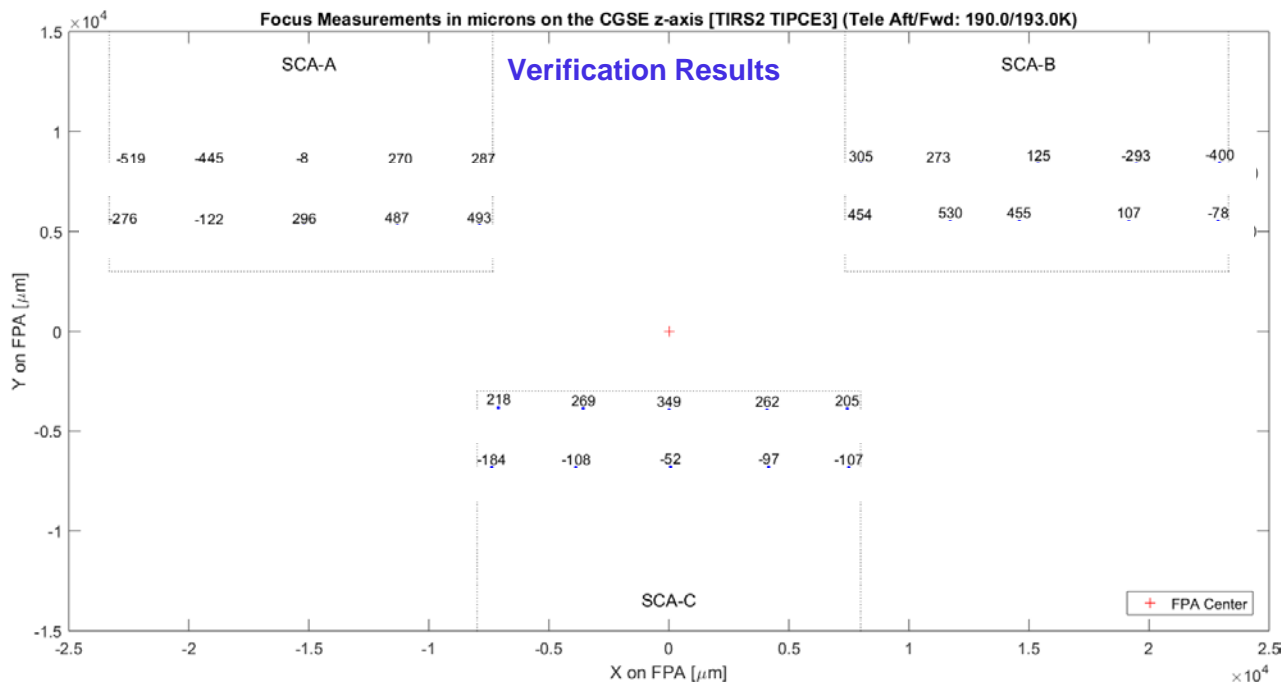


Focus Test Methodology



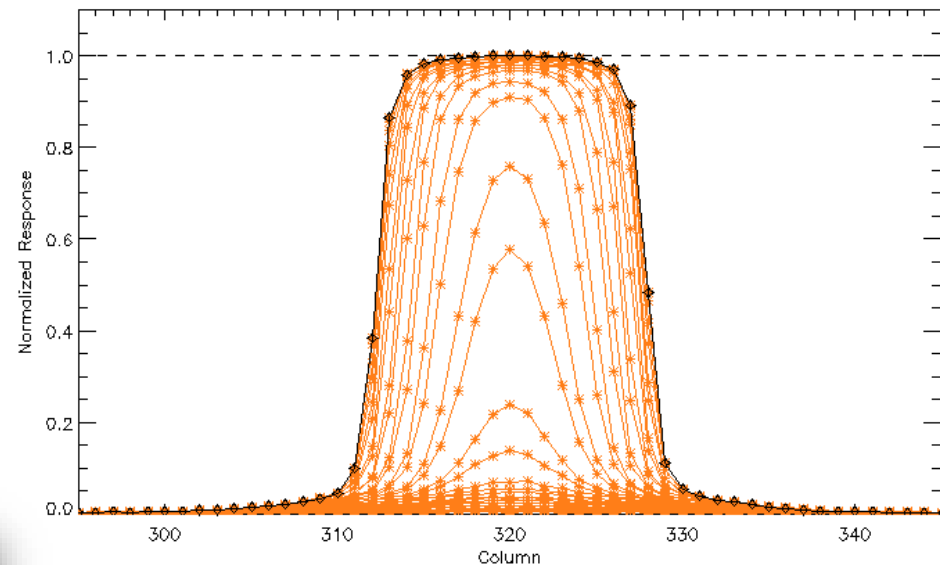
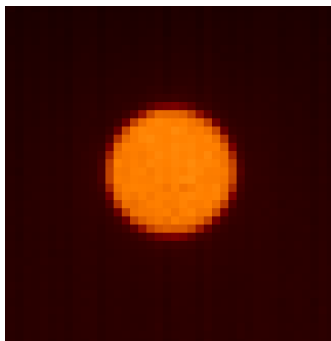
Focus Test Results

- Full focus survey collected during TIPCE with telescope at nominal temperature (190K/193K) - *Shims calculated, manufactured, and installed*
- Full focus survey for verification collected during another phase of TIPCE at nominal telescope temperature and at nominal +5 K.
 - Found average piston defocus of +90 microns of CGSE z-axis
 - shim deltas to be only: +0.0003", +0.0002", -0.0002"
 - **Decided on NO shim adjustment**
 - **Decided on NO telescope temperature adjustment**



- Processing follows the same methodology as used for TIRS1
 - Using ‘hockey puck’ target collect frames as target is moved in incremental sub-pixel (1/5) steps across-track and along-track over 3 pixels in each direction.
 - 16 pixel diameter circle target (“Hockey Puck”)
 - Large square for flat field
 - Blank for background correction
 - Repeat at different locations on FPA

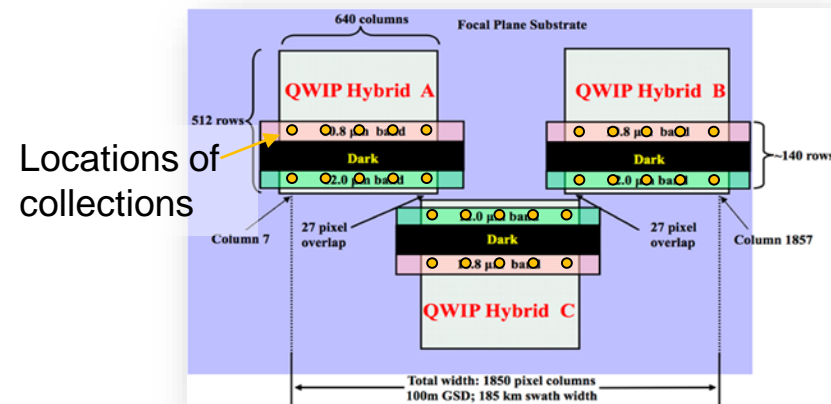
Raw image of ‘hockey puck’

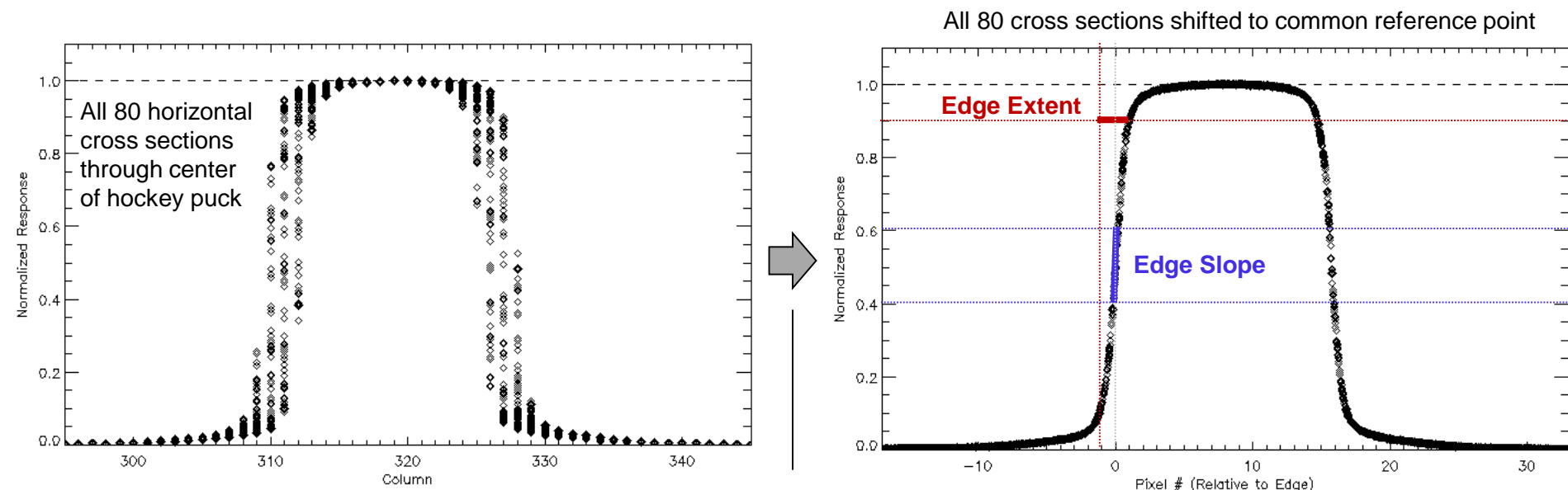


Each circular image frame has a background-correction and flat field applied at pixel level

$$dn(i,j) = (DN_P(i,j) - DN_{BKG}(i,j)) / (DN_{FF}(i,j) - DN_{BKG}(i,j))$$

Horizontal cross section through center of puck normalized to maximum value





Each frame fit with Fermi function to derive edge midpoint:

$$f(x) = \frac{a}{(e^{(x-b)/c}) + 1} + d$$

Each cross section shifted to match up mid-points resulting in a well populated edge

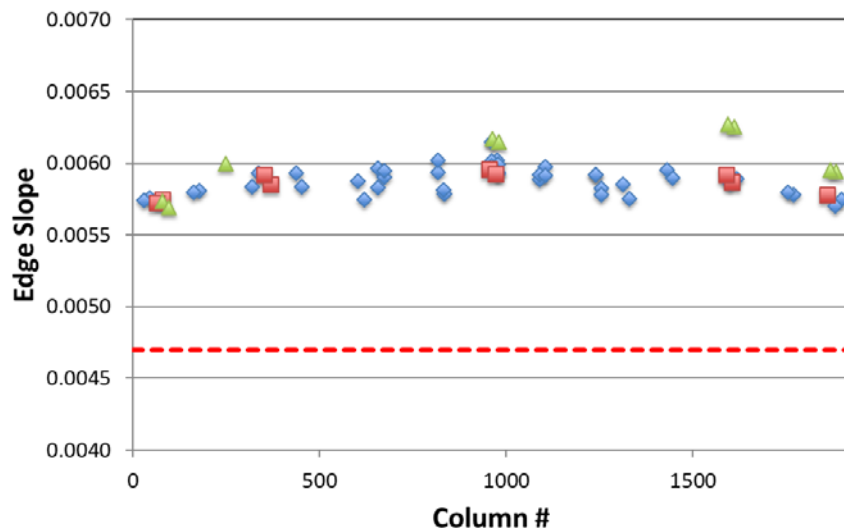
Metrics for evaluating spatial performance -- edge slope, edge extent -- derived from each edge response plot.



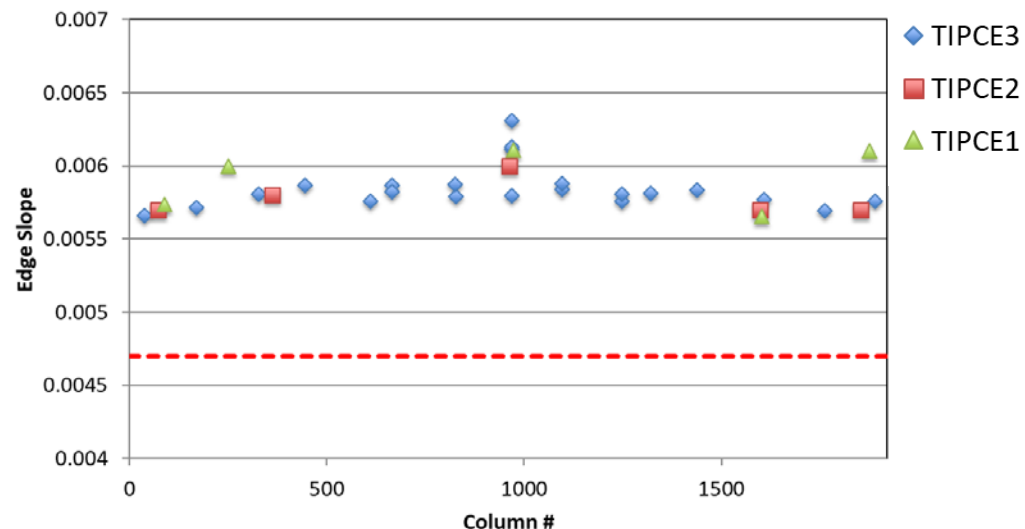
Spatial Response Results – Edge Slope



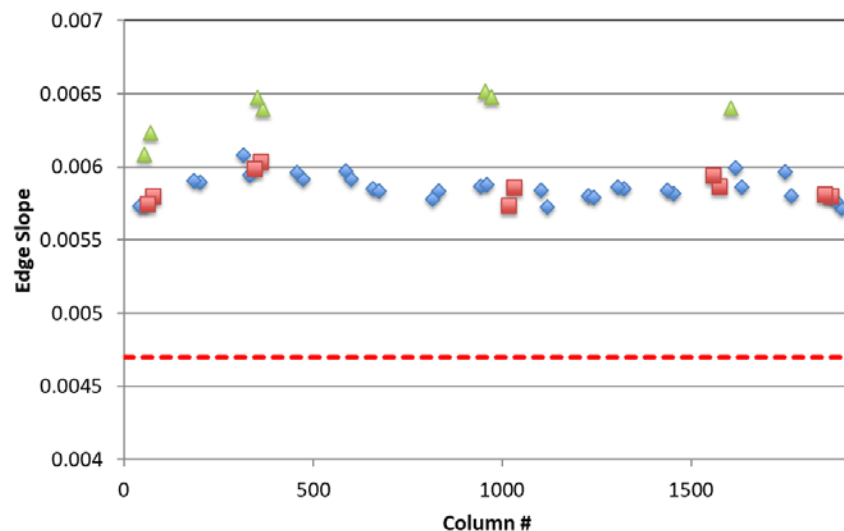
10.8 μm - Across Track



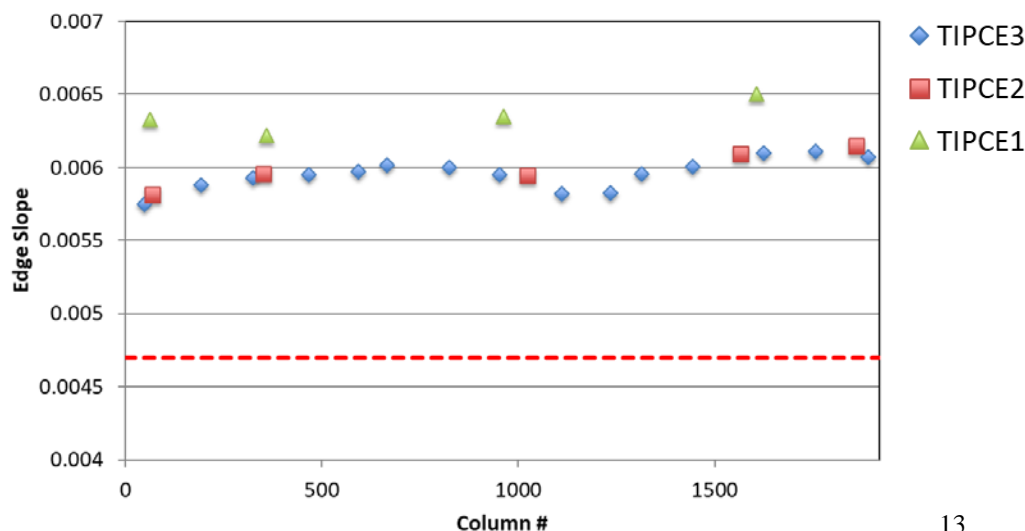
10.8 μm - Along Track



12.0 μm - Across Track



12.0 μm - Along Track

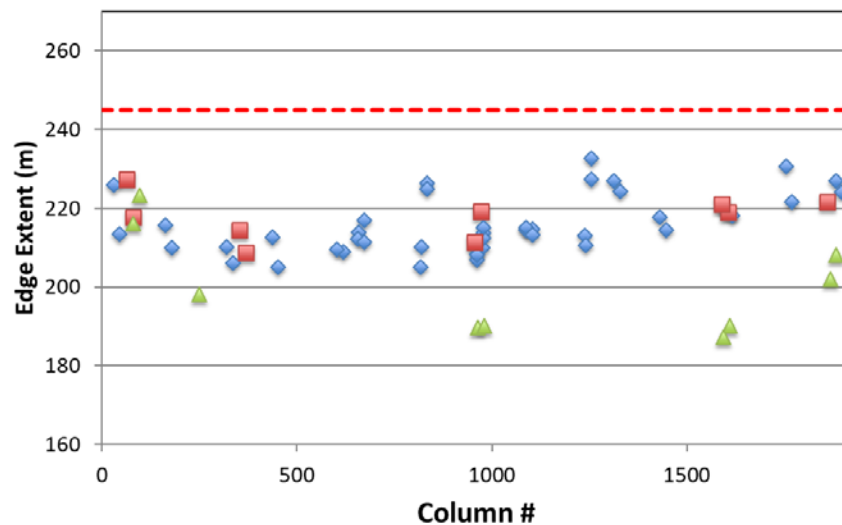




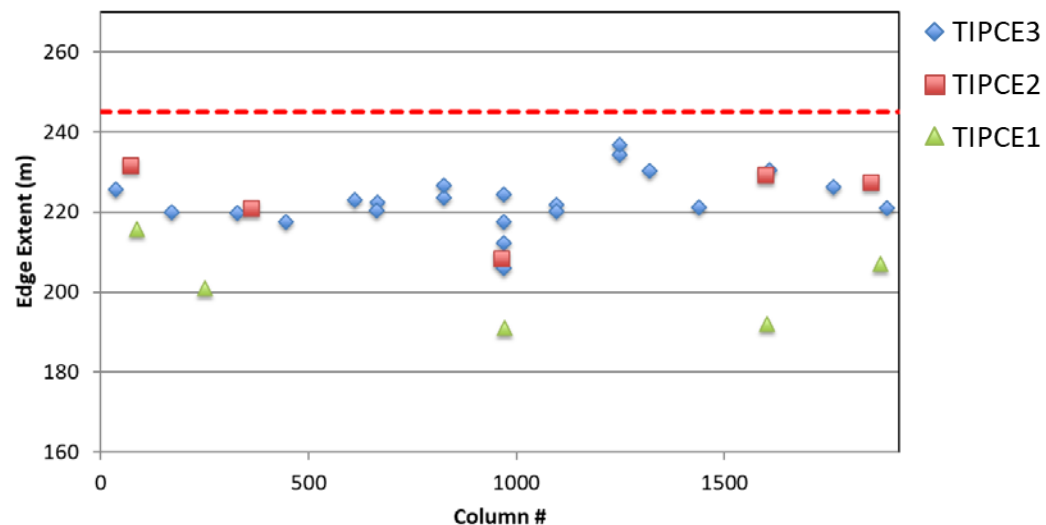
Spatial Response Results – Edge Extent



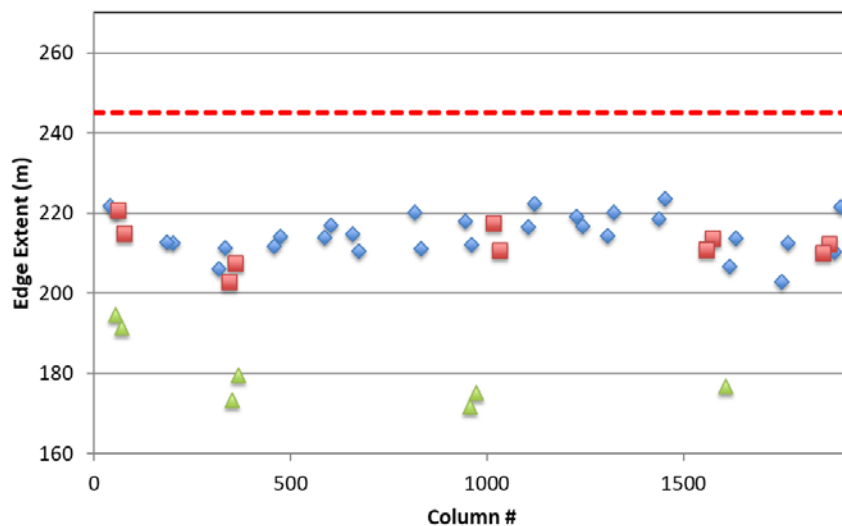
10.8 μm - Across Track



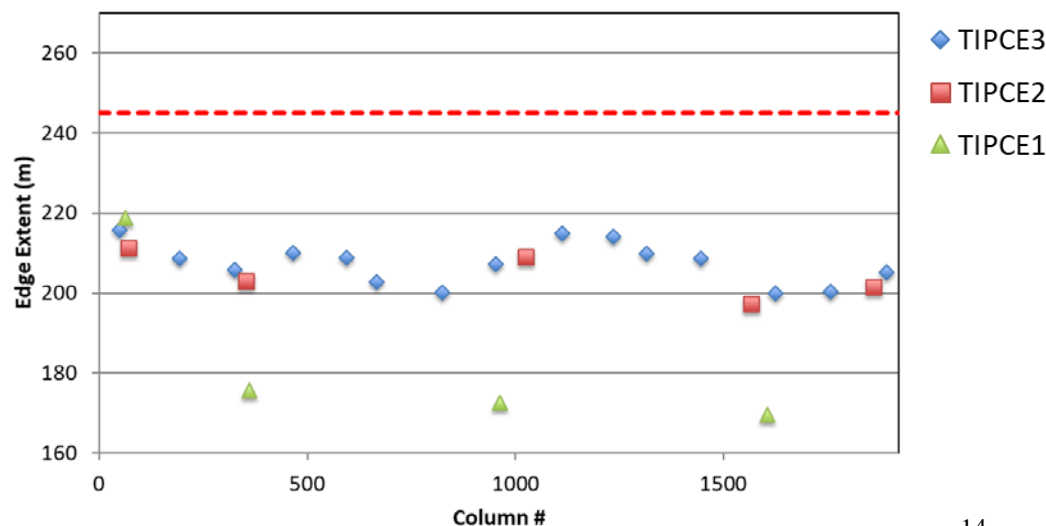
10.8 μm - Along Track



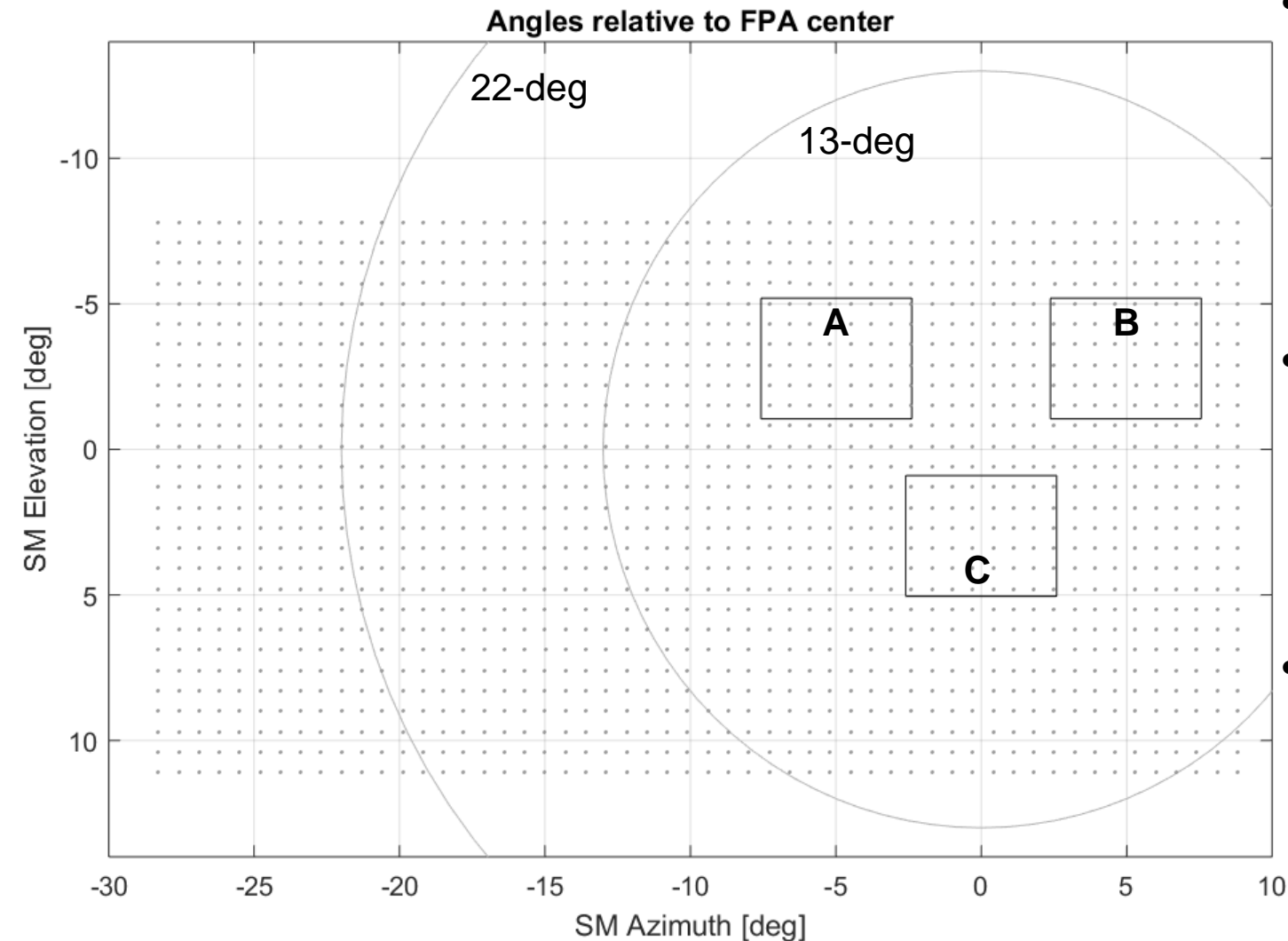
12.0 μm - Across Track



12.0 μm - Along Track



Scatter Scan Methodology

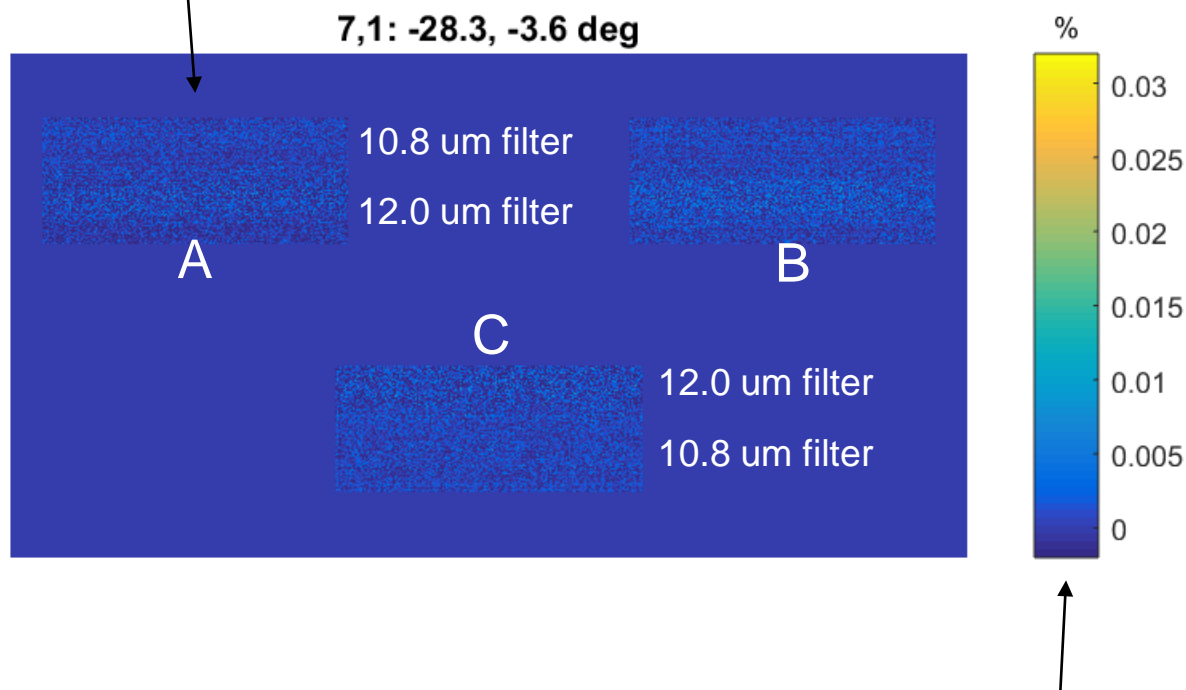
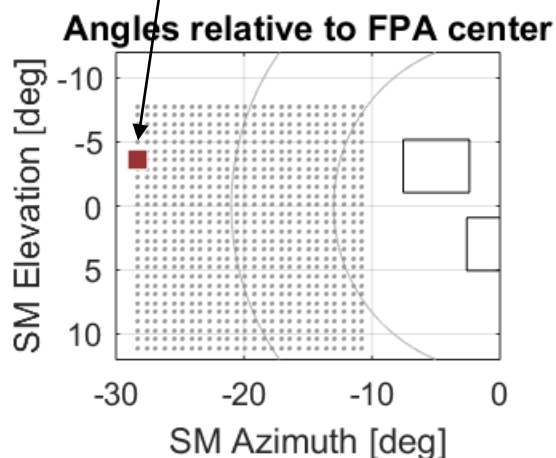


- Optical modeling reveals residual scattering at 13-deg and at 22-deg with the baffles.
- Wanted to scan the azimuthal extent of the 22-deg feature in TIPCE.
- Each dot represents the center of the 0.7-deg blackbody square target

Scatter Results: Target @ -28 deg

Blackbody square target is here

Frame of signal corresponding to the grid location

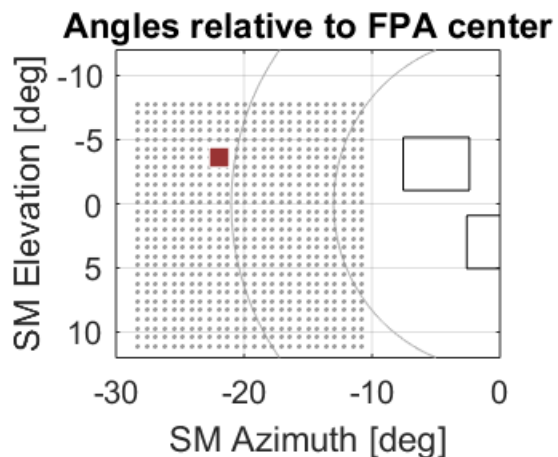


Units are percent of the signal when the target is directly illuminated on the detectors

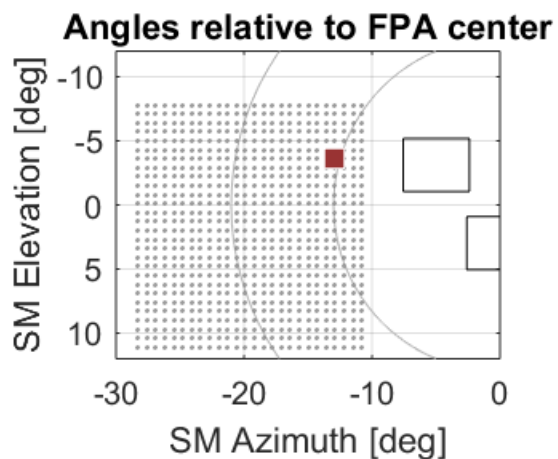


Scatter Results:

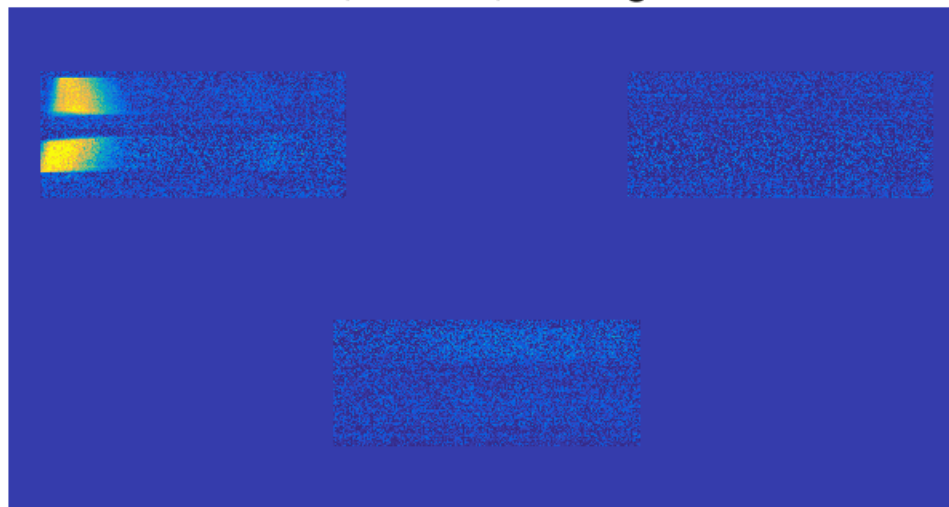
Target @ -22 deg and @ -13 deg



7,10: -22.0, -3.6 deg

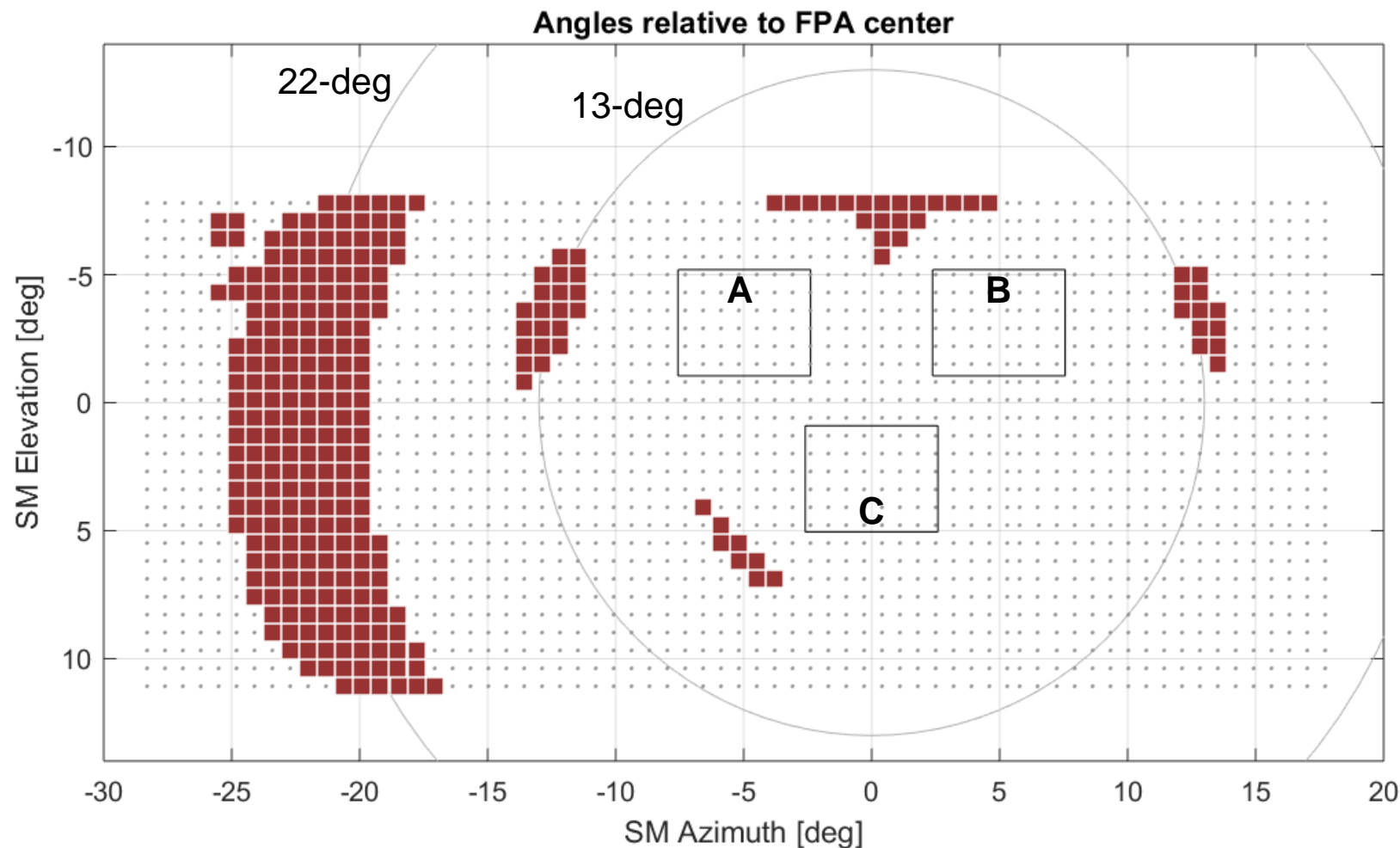


7,23: -12.9, -3.6 deg



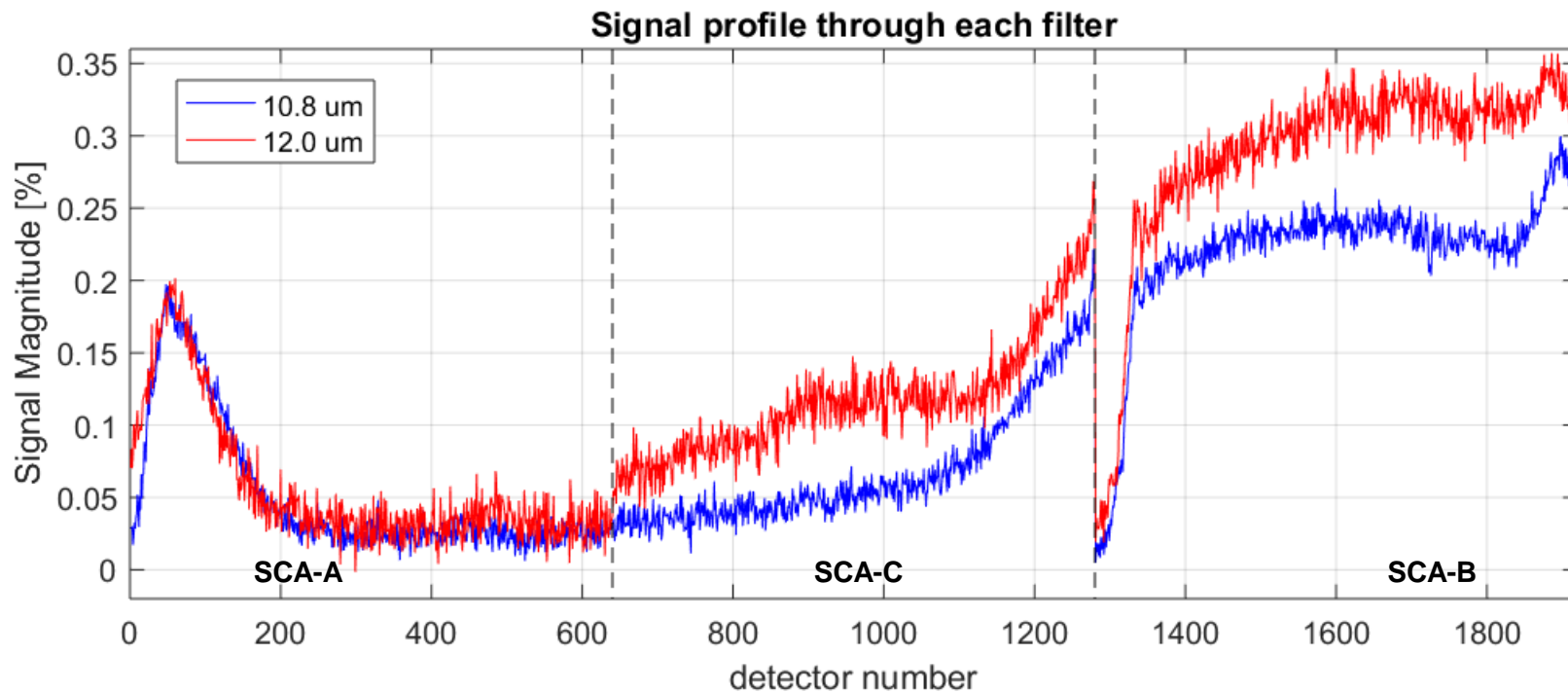
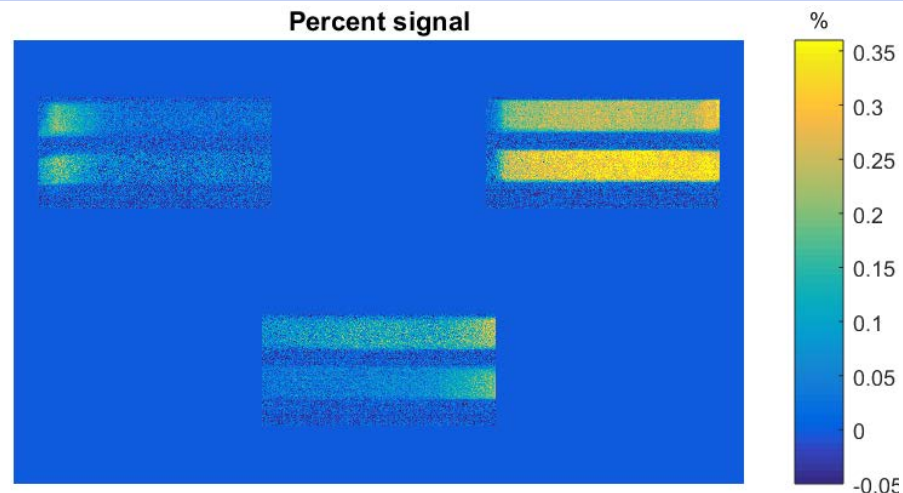
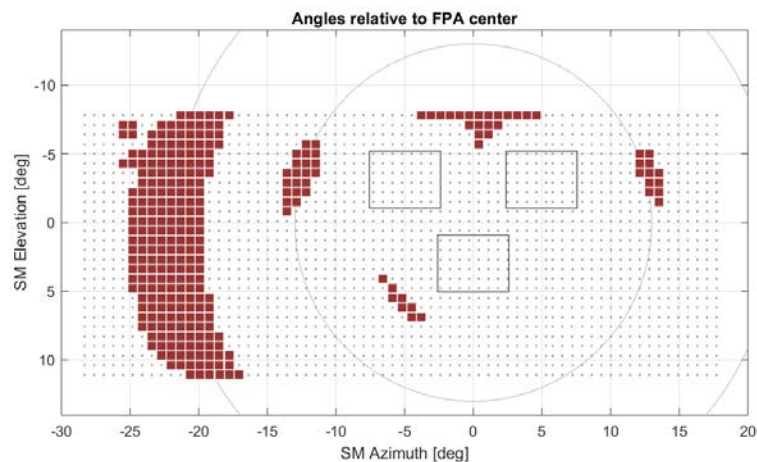
Scatter Results: Total Scattering

- Combine scattering data from TIPCE2 and TIPCE3. Red boxes where source was when signal observed on any detector.





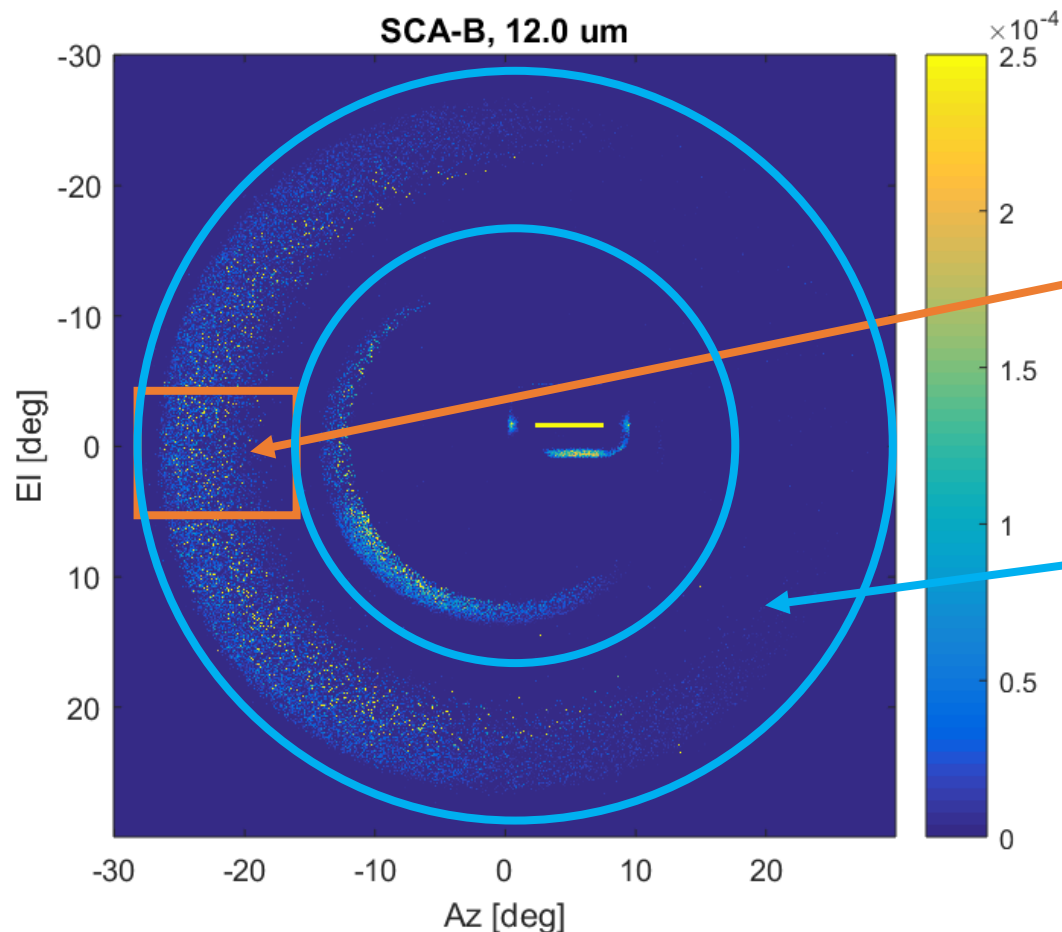
Scatter Results: TIPCE Scattering Sum



Scatter Results:

TIPCE3 Scatter vs. Optical Model

Optical model from June Tveekrem for SCA-B, 12 μm band



- TIPCE angles do not encompass entire out-of-field but can use TIPCE results to scale optical model to same units.
- Use sum of TIPCE signal here and sum of model signal here to derive scale factor
- Scale entire optical model using scale factor and sum up signal for each SCA/band.



Scatter Results: Total Scatter Sum



- Sum using optical model :

	10.8 um	12.0 um
SCA-A	0.69 %	1.11 %
SCA-B	0.76 %	1.01 %
SCA-C	0.24 %	0.21 %

- Preliminary look at science impact:

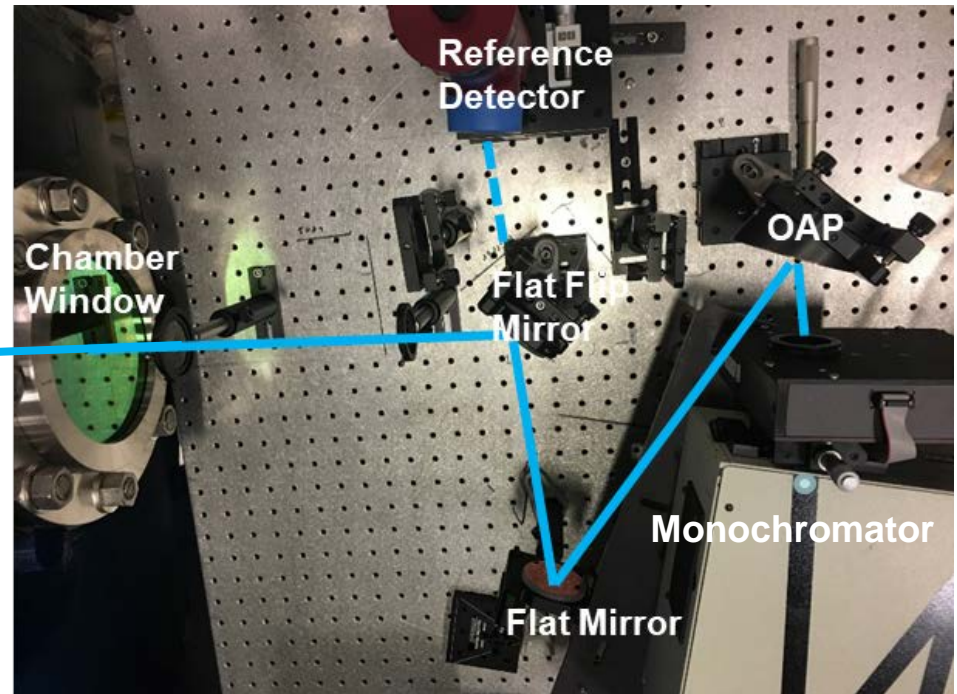
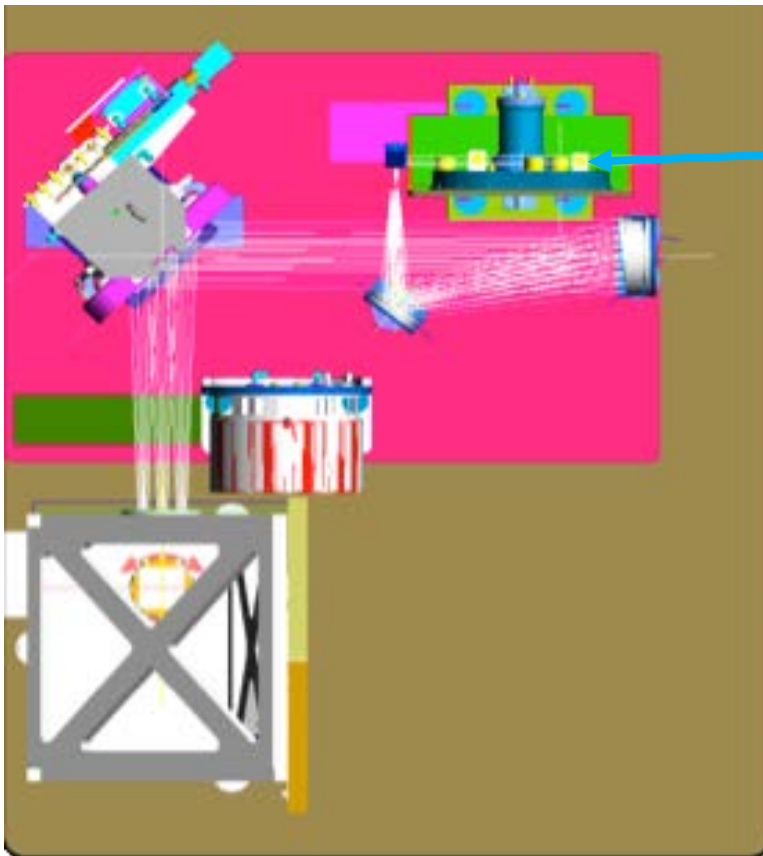
SCA-A, 12.0 um, 1.11%

Out-of-field Temperature is:

In-field Temperature is:		200	240	260	270	280	290	300	320	330
	240	-2.06	-1.36	-0.83	-0.52	-0.18	0.19	0.59	1.48	1.97
	260	-1.40	-0.92	-0.56	-0.35	-0.12	0.13	0.40	1.00	1.33
	270	-1.18	-0.77	-0.47	-0.30	-0.10	0.11	0.34	0.84	1.12
	280	-1.00	-0.66	-0.40	-0.25	-0.09	0.09	0.29	0.72	0.96
	290	-0.86	-0.57	-0.35	-0.22	-0.08	0.08	0.25	0.62	0.82
	300	-0.75	-0.49	-0.30	-0.19	-0.07	0.07	0.21	0.54	0.72
	310	-0.66	-0.43	-0.26	-0.17	-0.06	0.06	0.19	0.47	0.63
	320	-0.58	-0.38	-0.23	-0.15	-0.05	0.05	0.17	0.42	0.55
	330	-0.52	-0.34	-0.21	-0.13	-0.05	0.05	0.15	0.37	0.49
	360	-0.38	-0.25	-0.15	-0.10	-0.03	0.03	0.11	0.27	0.36

Numbers in table are the percent radiance that the condition is high or low when an out-of-field radiance of 285 K is assumed and removed from the calibration.

- Data collect with TIRS from the monochromator bracketed by collects with the MCT reference detector
- Cal GSE in “monochromator mode” where collimated beam from the setup outside the chamber is focused and then re-collimated



$$dn_{corr}(\lambda, pix) = \frac{\text{Background subtracted TIRS counts} \times \text{reference path transmittance}}{\text{TIRS path transmittance} \times \text{TIRS reference detector signal}}$$

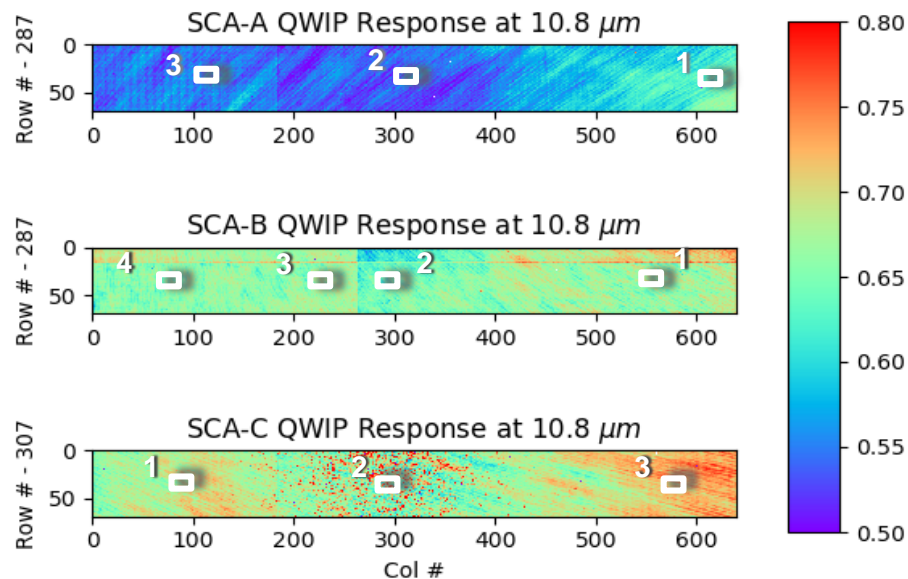
$$dn_{corr}(\lambda, pix) = \frac{dn_{TIRS}(\lambda, pix) \times \tau_{ref\ path}}{\tau_{TIRS\ path} \times V_{ref}}$$

$$RSR_{TIRS}(\lambda, pix) = \frac{dn_{corr}(\lambda, pix)}{\max_{\lambda}(dn_{corr}(\lambda, pix))}$$

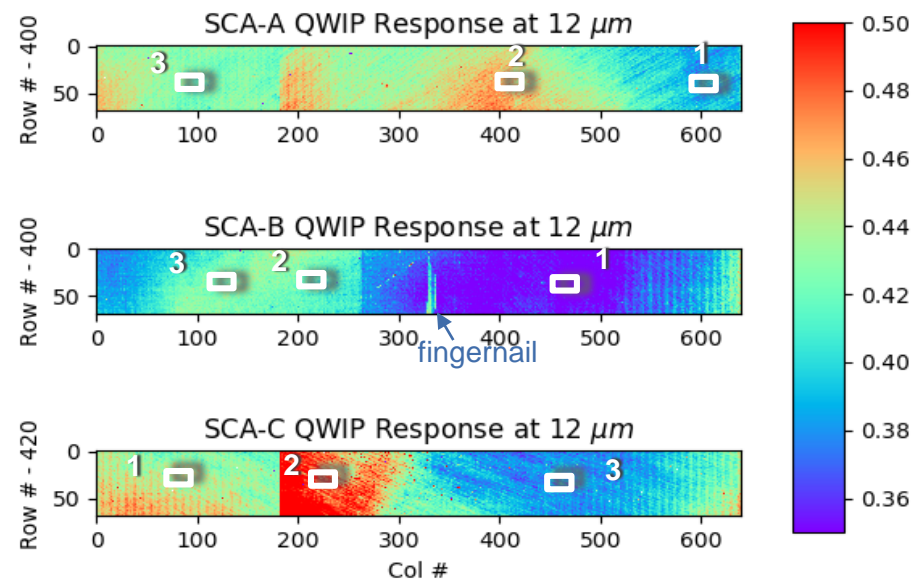
Spectral Response Test Methodology

- Data was collected for three or four locations on each SCA.
- The monochromator slits were 2 mm.
- TIRS data is collected using the monochromator shutter to provide background measurement. MCT data is collected between channels/SCAs.
- Optimization of the linear stage is run before each collect.
- Optimized for integration time

10.8 μm

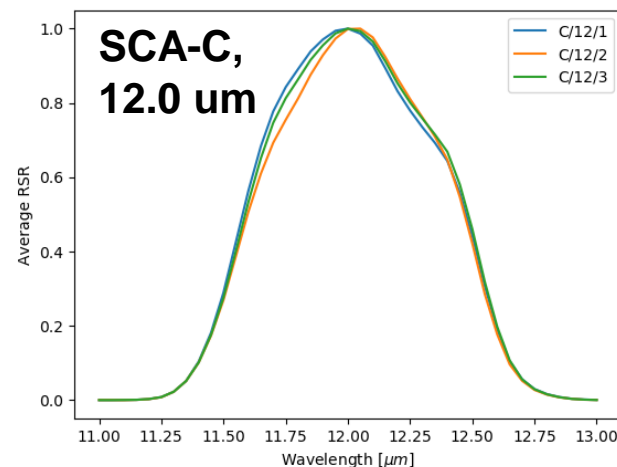
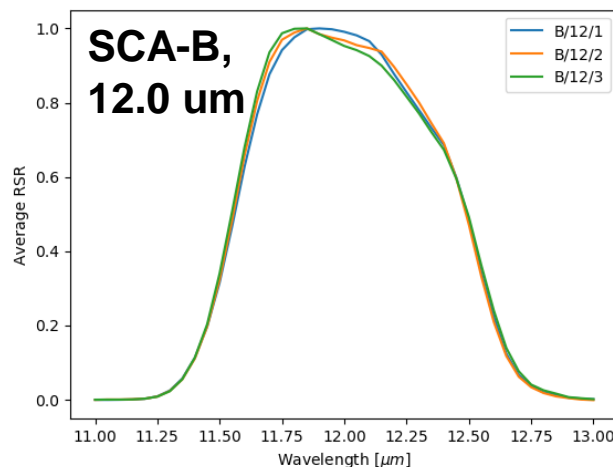
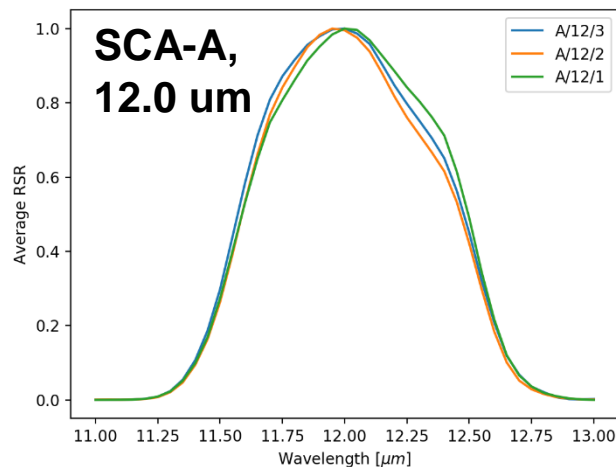
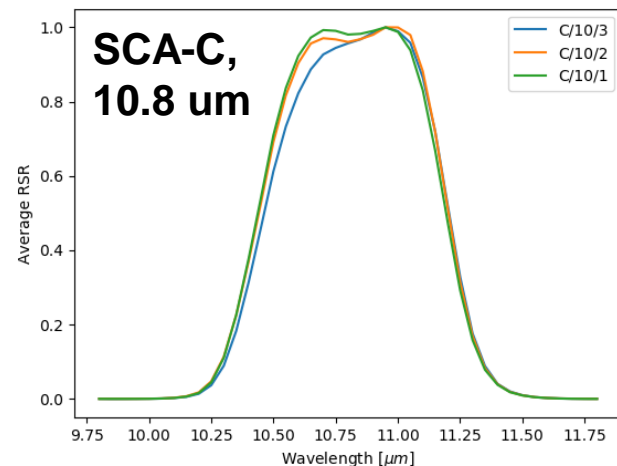
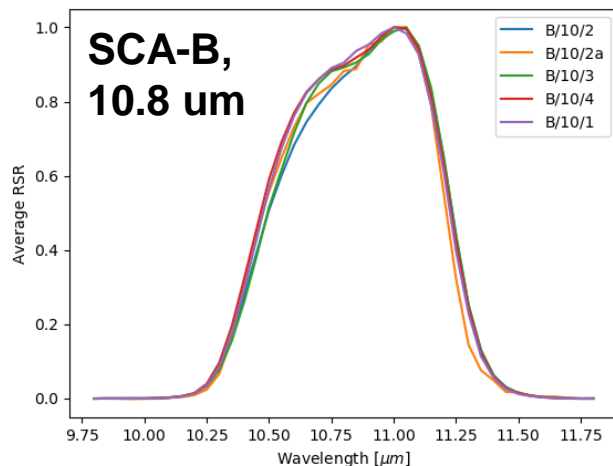
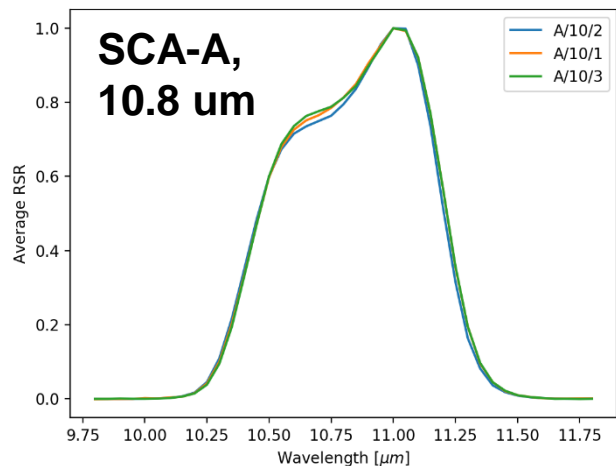


12.0 μm





Spectral Response Results

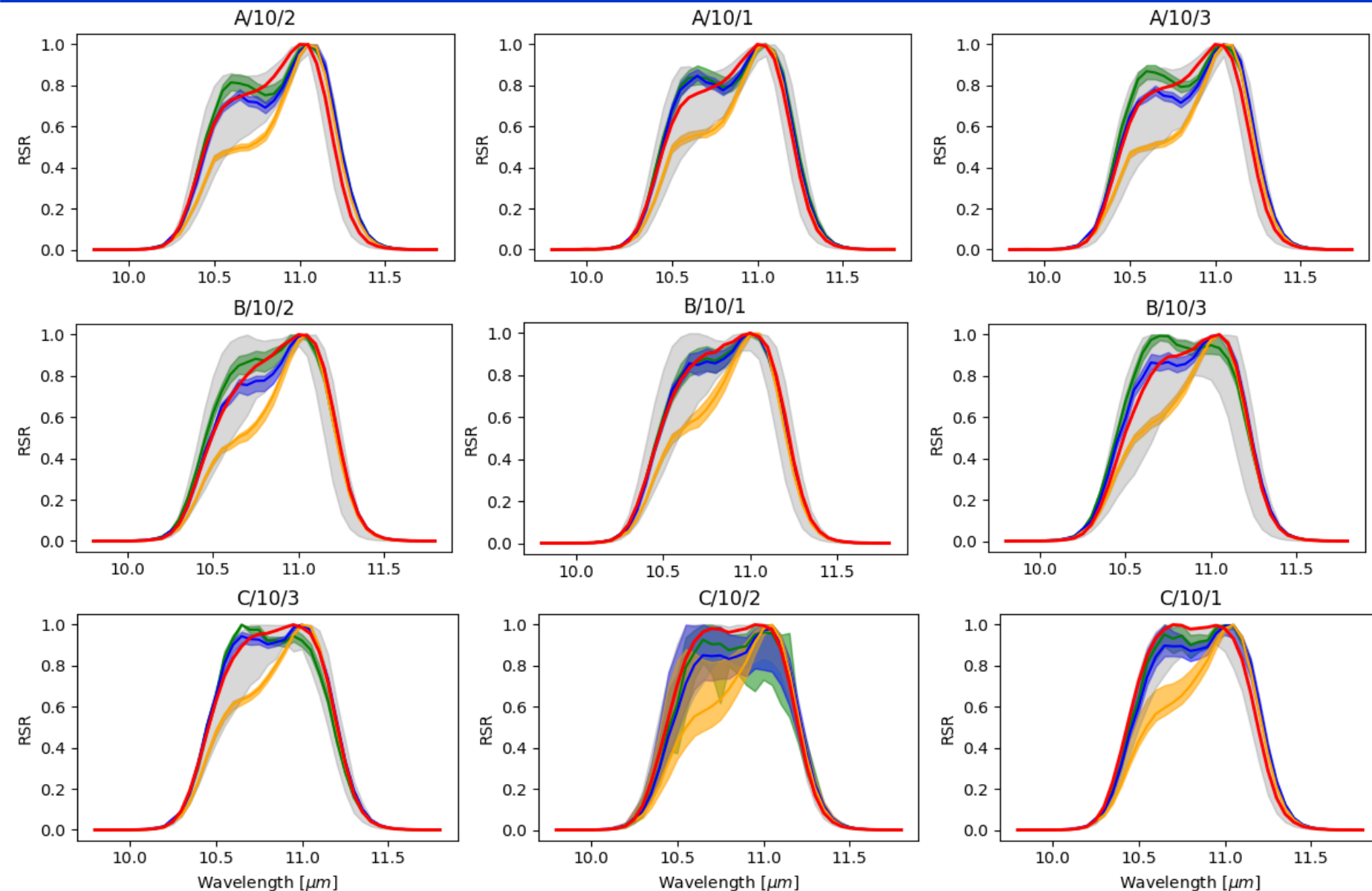




Spectral Response Results: Comparison to Component-Level 10.8 μm



FPA-level (F/1.6) SCA-level (F/1.6) SCA-level. (Normal Inc.) TIPCE3

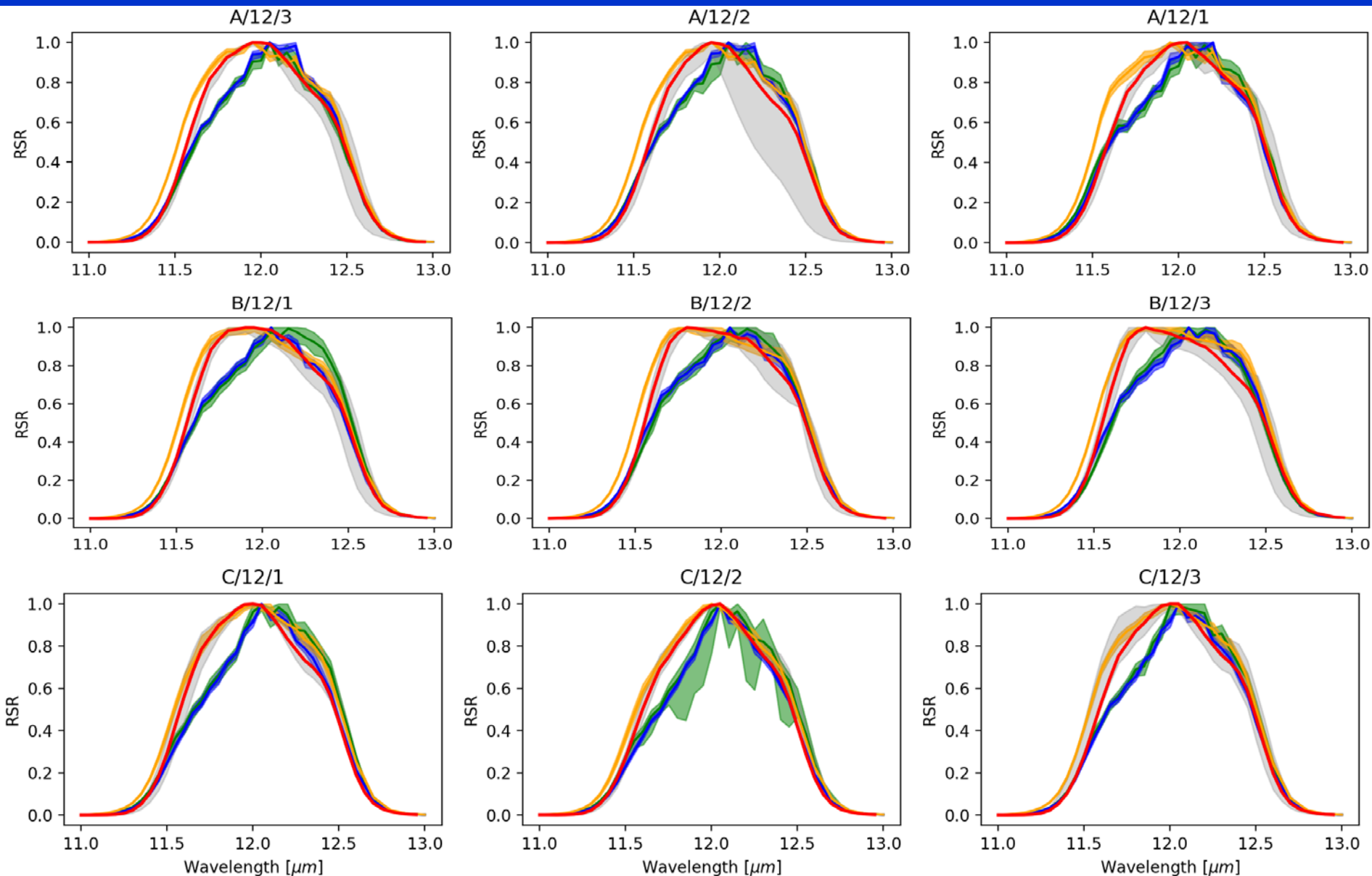




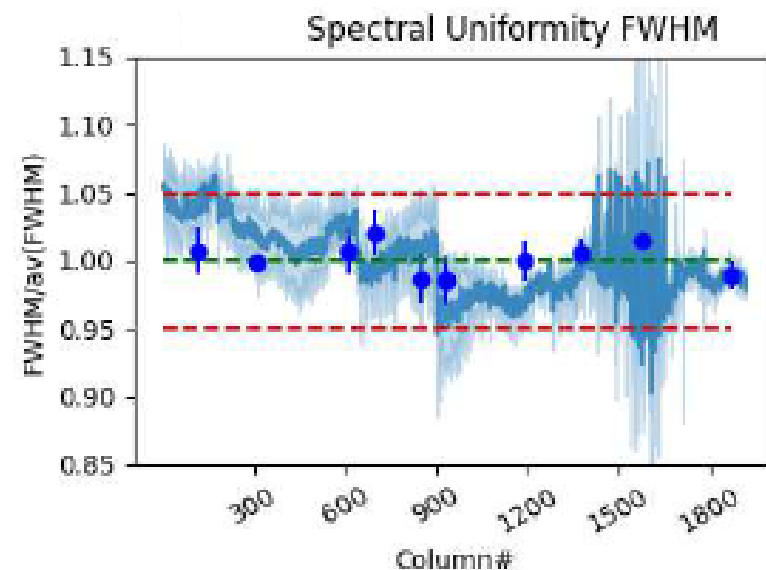
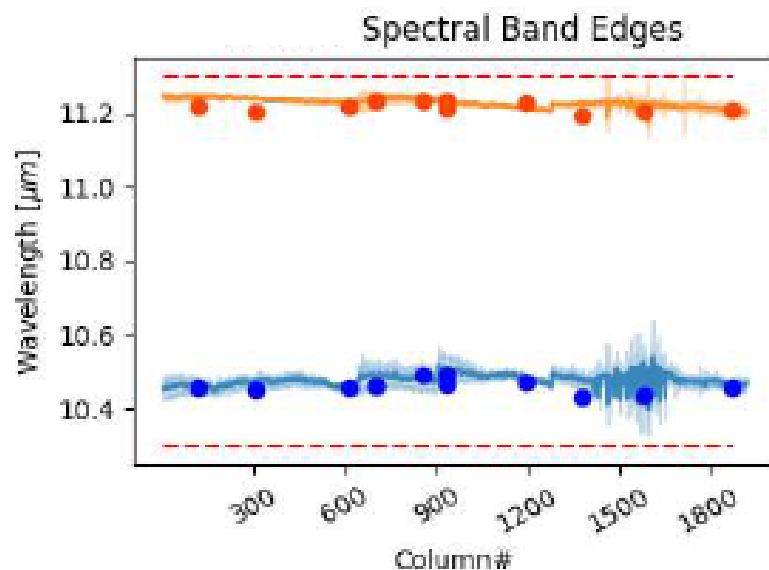
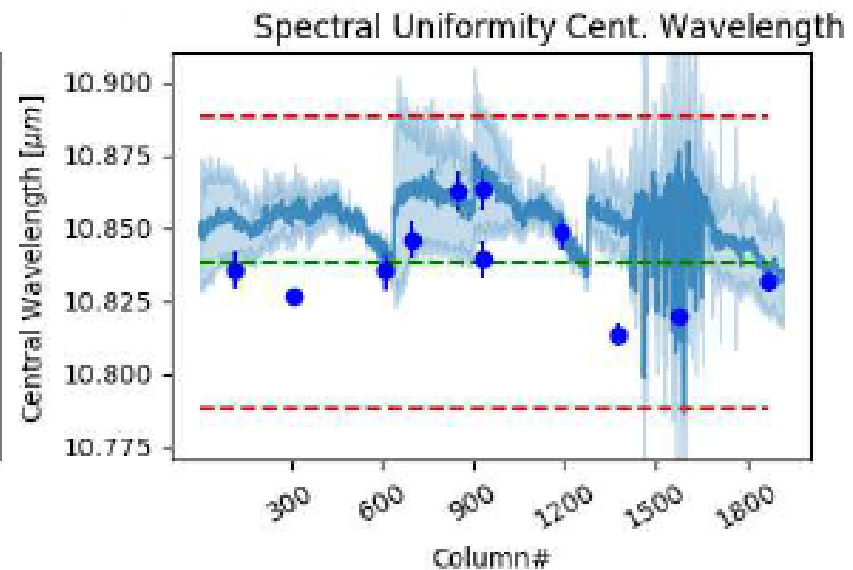
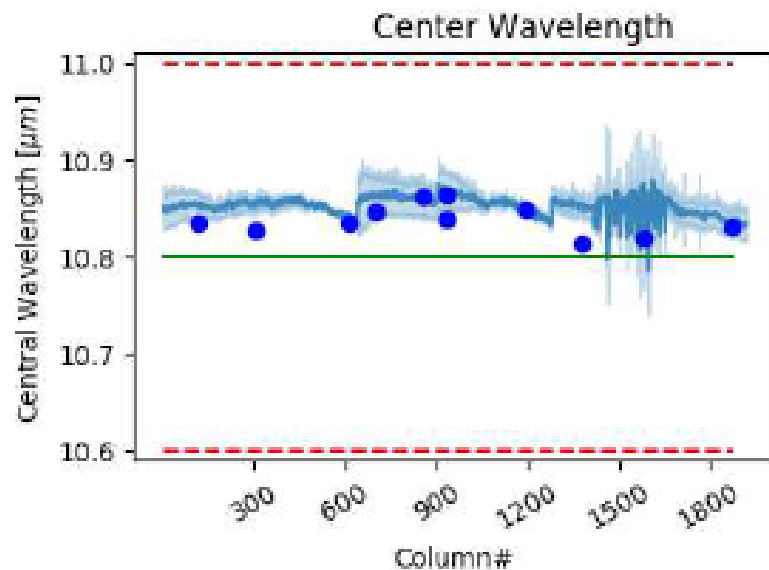
Spectral Response Results: Comparison to Component-Level 10.8 μm



FPA-level (F/1.6) SCA-level (F/1.6) SCA-level. (Normal Inc.) TIPCE3

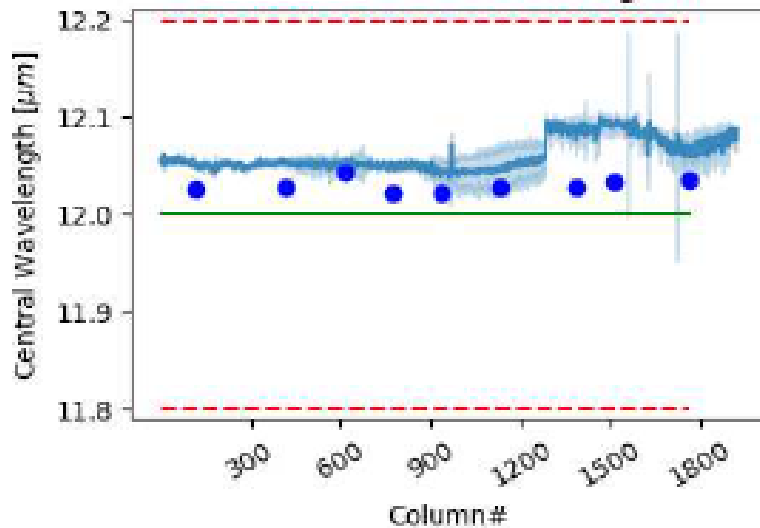


Spectral Response Results: Requirements 10.8 μm

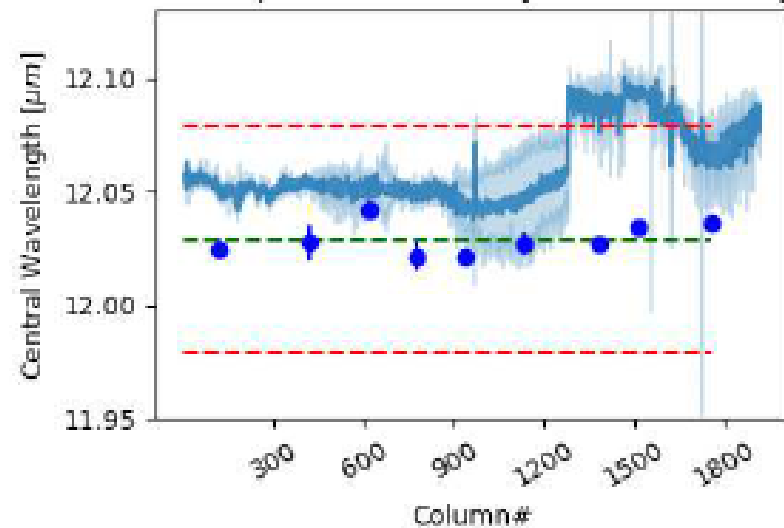


Spectral Response Results: Requirements 12.0 μm

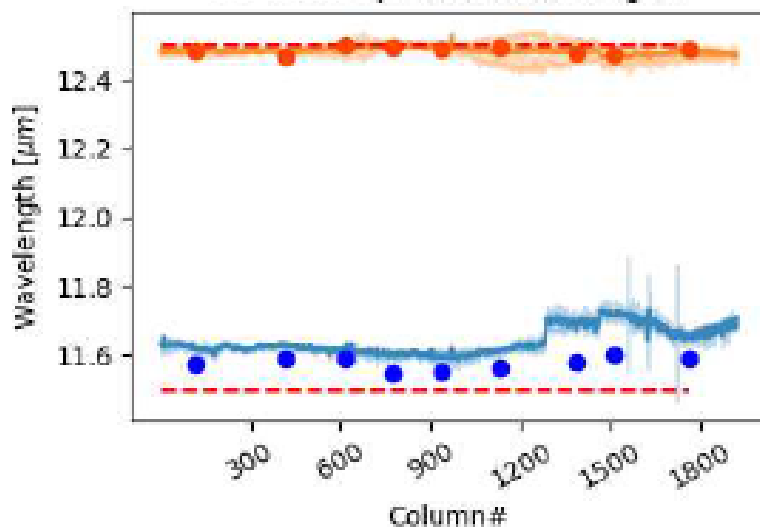
Center Wavelength



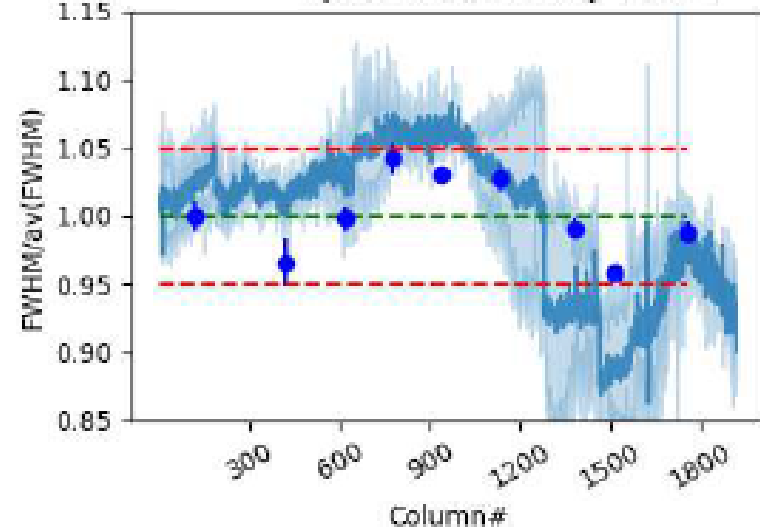
Spectral Uniformity Cent. Wavelength



Spectral Band Edges



Spectral Uniformity FWHM





Summary



- The results show that TIRS-2 performance is expected to meet all of its performance requirements with few waivers and deviations.
 - Initial TIRS-2 performance testing set and verified the focus of the instrument.
 - Spectral response results show good agreement with component-level measurements accounting for the angular dependence of the detector spectral response.
 - The scatter survey showed improved stray light rejection compared to TIRS-1 the total stray light effect of 1% or less (TIRS-1 – 8%).
- Current preparations for instrument-level thermal vacuum in the fall testing are now underway and delivery is expected Aug 2019.



Backup

Spectral Shape Setup – Monochromator Wavelength Calibration/Validation

- Used NIST wavelength standard (1921b) to calibrate the monochromator wavelength scale using absorption lines closest to the TIRS-2 bands
- The adjustment was programmed into the monochromator to correct an 120 nm offset before TIPCE
- The wavelength calibration was validated pre/post TIPCE phases**
 - Monochromator wavelength < 10 nm from wavelength reference throughout TIPCE.**

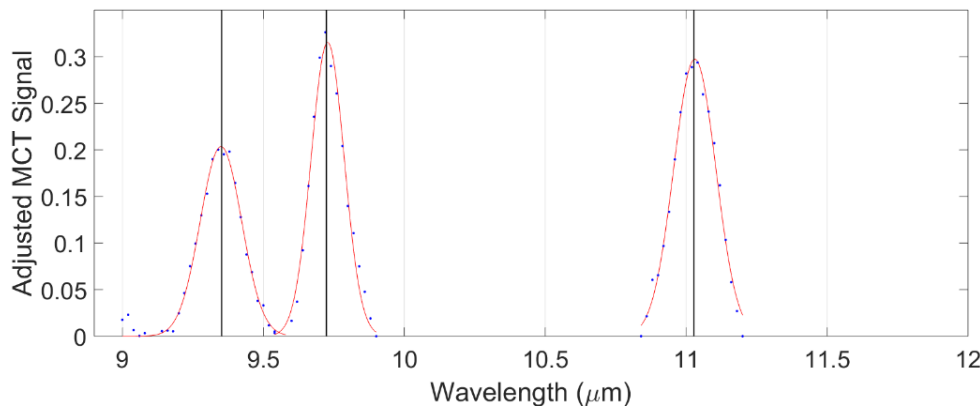
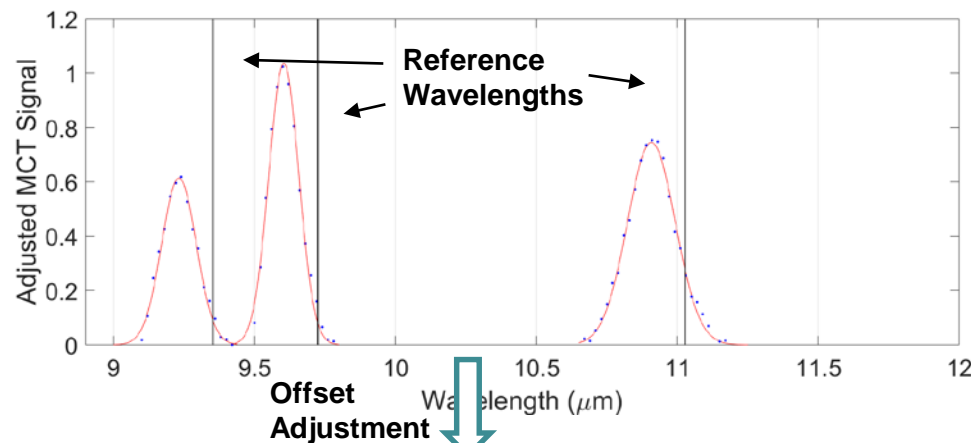


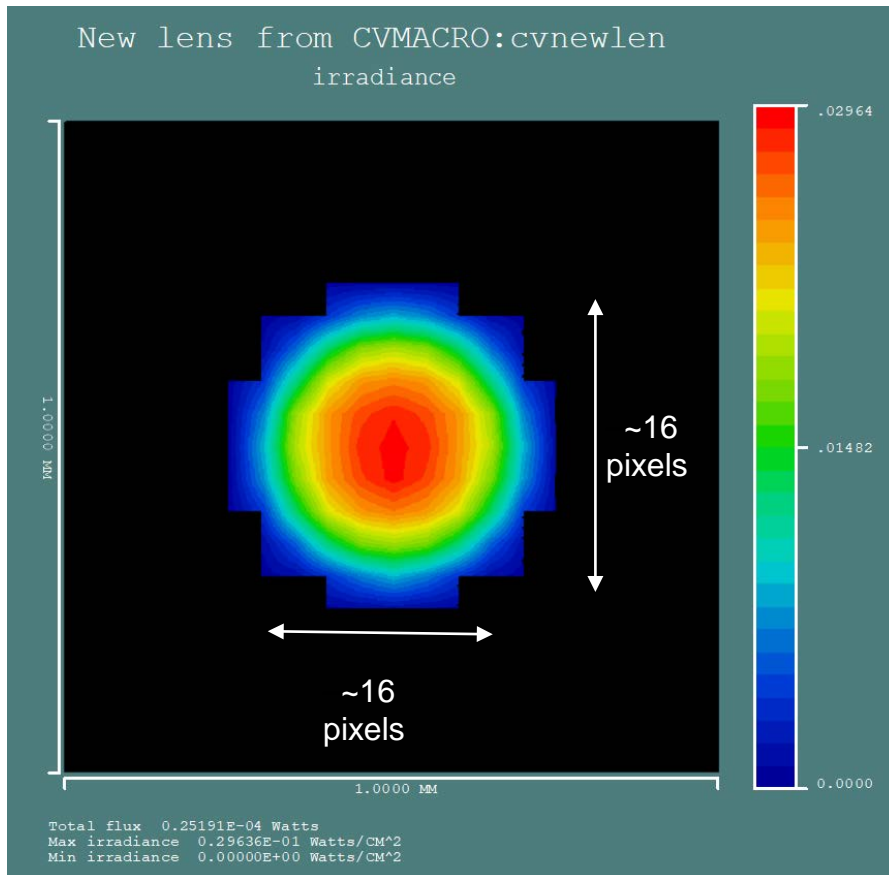
Table 1. Certified Band Centroid Wavelength Values (in Vacuum)

Band Number	Band Wavelength (μm)	Expanded Uncertainty, U (μm)
1	18.3512	8.2×10^{-2}
2	11.8751	1.8×10^{-2}
3	11.0276	1.3×10^{-3}
4	9.7237	2.5×10^{-3}
5	9.3522	6.8×10^{-3}
6	8.6608	7.0×10^{-4}
7	6.3169	3.4×10^{-4}
8	6.2446	4.1×10^{-4}
10	3.50853	1.5×10^{-4}
11	3.33178	1.0×10^{-4}
12	3.30421	1.0×10^{-4}
13	3.26782	9×10^{-5}
14	3.24442	1.0×10^{-4}

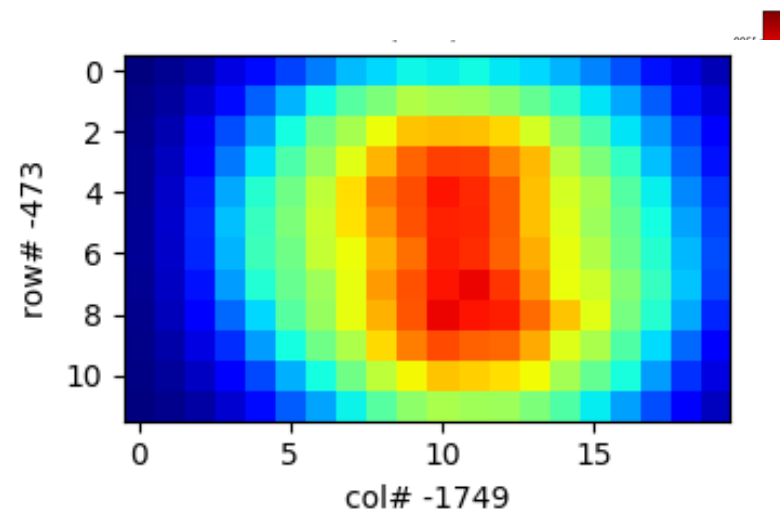
NIST Certificate SRM 1921b



Simulated Image on TIRS focal plane

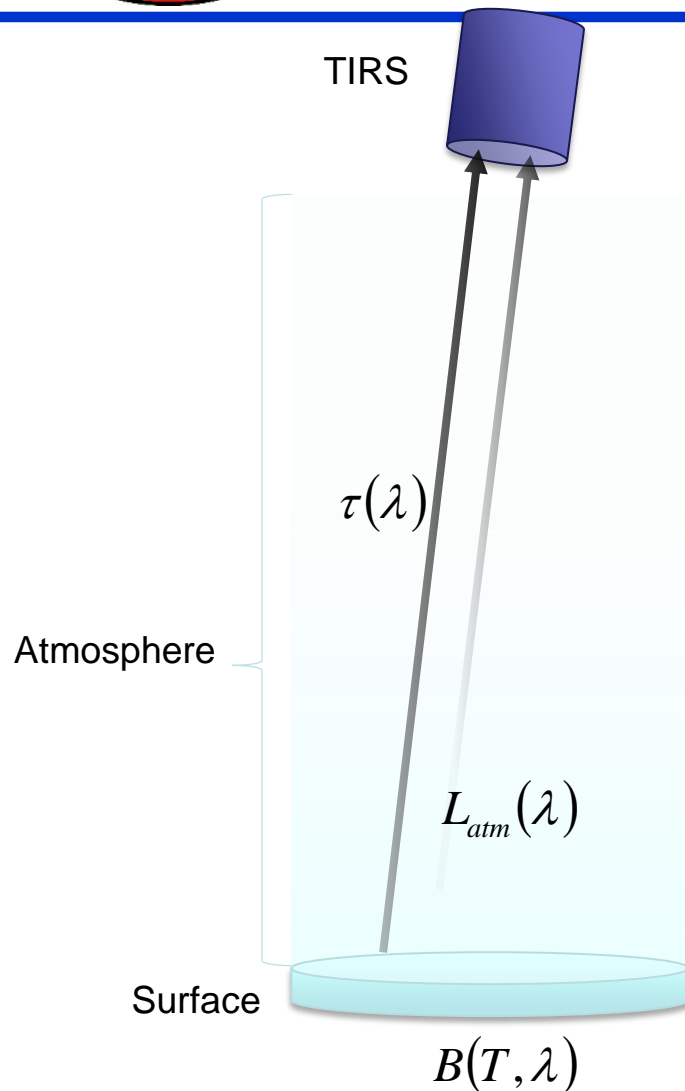


Measured Image on TIRS focal plane



Model and TIPCE
show slit images with
similar shapes & sizes

Thermal Radiance Detected by TIRS-2 from Surface and Atmosphere



$$L_s = \frac{\int (B(T, \lambda) \cdot \tau(\lambda) + L_{atm}(\lambda)) \cdot R'(\lambda) \cdot d\lambda}{\int R'(\lambda) \cdot d\lambda}$$

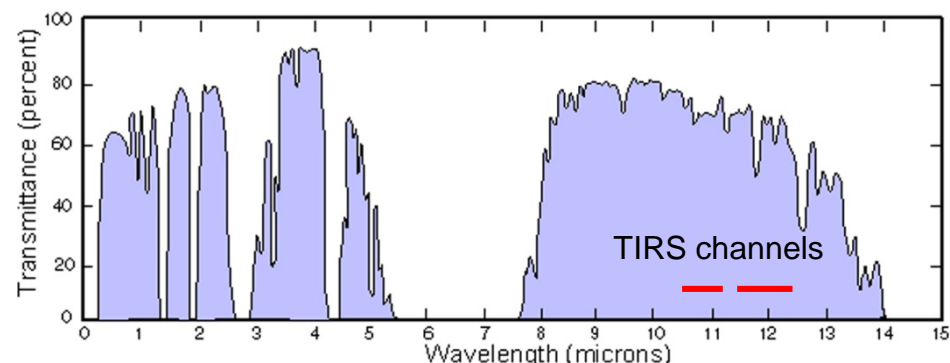
$B(T, \lambda)$ • Emitted and reflected surface radiance

$\tau(\lambda)$ • Transmission of atmosphere

$L_{atm}(\lambda)$ • Emitted and scattered radiance of atmosphere

$R'(\lambda)$ • Spectral response of pixel

L_s • Pixel integrated radiance



Two channel “split window” techniques correct for atmosphere and improve retrieved surface temperature